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The Education, Scholarships, Apprenticeships and Youth Entrepreneurship

EUROPEAN NETWORK FOR 3D PRINTING OF BIOMIMETIC MECHATRONIC SYSTEMS

E-toolkit for teaching purposes, basic knowledge about realizing biomimetic mechatronic systems

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CONTENT

Computer Aided Design (CAD)
Computer Aided Engineering (CAE)
3D Printing
New materials used for the developed biomimetic mechatronic systems
Virtual Reality/ Augmented Reality











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EUROPEAN NETWORK FOR 3D PRINTING OF BIOMIMETIC

MECHATRONIC SYSTEMS

E-toolkit – Computer Aided Design

| Project Title | European network for 3D printing of biomimetic mechatronic systems 21-COP-0019 | |
|------------------|---|--|
| Output | IO2 - EMERALD e-toolkit manual for digital learning in producing biomimetic mechatronic systems | |
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| 1 | Introduct | tion | |
|---|-----------|---|----|
| | | | |
| 2 | Design of | f mechanical part of the prosthesis | 4 |
| | 2.1 N | fain assumptions | 4 |
| | 2.2 G | enerative CAD model – principles of operation | 4 |
| | 2.3 P | rosthesis model design | 6 |
| | 2.3.1 | Prosthetic socket | |
| | | Forearm End effector | |
| | | | |
| | 2.4 F | inal version of bicycle prosthesis | 21 |
| | 2.5 D | esign of electronic part of the biomechatronic prosthesis | 25 |
| | 2.5.1 | Main concept of the mechatronic prosthesis | |
| | 2.5.2 | Design modifications in biomechatronic prosthesis | 26 |
| 3 | Summary | V | 28 |











1 Introduction

This toolkit presents practical information on how to a CAD model of a biomechatronic hand prosthesis can be built and structured. An example of modular prosthesis will be considered, with its adjustment to needs and preferences of an adult patient and converting static mechanical device into a mechatronic prosthesis, equipped with sensors for monitoring the activities performed by prosthesis user.

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2 Design of mechanical part of the prosthesis

2.1 Main assumptions

The prosthesis has been prepared for continuous and demanding cycling for an adult patient. The modular mechanical prosthesis was originally generated automatically for the child. Then, the necessary changes were made to adapt it to an adult. After testing and optimizing the bicycle, the adult mechanical prosthesis was transformed into a mechatronic one through sensorization.

The modular model of the prosthesis has been described in multiple previous work by the team of authors [1-2], or supervised by them (Master's thesis [3] and [4]). Most of the descriptions in this chapter come from these works, as well as previously undisclosed project reports.

2.2 Generative CAD model – principles of operation

In this work, a project of an intelligent model of the upper limb prosthesis was implemented, which is characterized by a modular structure. The device is an integrated whole composed of many components with unified terminals. The model is loaded with anthropometric and configuration data directly from an external Excel file, enabling both the generation of anatomically matched prosthesis components and the manipulation of its variants to create any combination of all parts. Therefore, the model allows for the quick and fully automated production of many configurations of individualized prostheses for the same or many different patients. The architecture of the modular model is shown in Figure 1.

The concept of the model was made as part of the project "Automation of design and rapid production of individualized orthopedic and prosthetic products based on data from anthropometric measurements", serving the development of the prototype AutoMedPrint system built at the Faculty of Mechanical Engineering of the Poznań University of Technology.











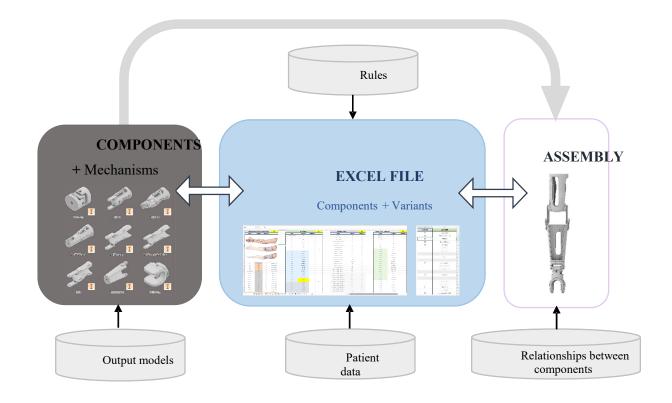


Figure 1 Architecture of the designed system [3]

The model consists of three types of main components - sockets, forearms and effectors. Types of individual elements of a given type are presented in Table 1. However, the modular prosthesis also includes sacroiliac joints (cardans) that function as a movable wrist joint, an assembly adapter and an elbow module that imitates flexion and extension in the frontal plane.







Table 1 List of components of the modular model

| | Prosthetic sockets | Prosthetic forearms | Effectors | | |
|---|--|---|---|--|--|
| | CRS compression and relaxation socjet (4 variants) Open socket (2 variants) Semi-open socket (3 variants) CRS socket for amputation within the forearm | Forearm open Open forearm with a tip dedicated to the adapter Closed forearm with a tip dedicated to the adapter Forearm completely closed with a tip dedicated to the adapter | C-Handle Fixed straight handle Fixed angular handle Straight handle with a spring A mechanical hand | | |
| | Connecting and auxiliary elements | | | | |
| _ | Cross joints 2 adapters | External model of the elbow A shaped piece that blocks the elbow joint | | | |

All elements are designed from the beginning in a parametric angle, making the dimensions of the elements dependent on anthropometric measurements from scans of healthy upper limbs of patients.

2.3 Prosthesis model design

2.3.1 Prosthetic socket

The first stage of creating an autogenerating model of upper limb prostheses was modeling the structure of the prosthetic socket. The socket is generated on the basis of data from spatial scanning of the patient's residual limb. The algorithm developed by the team of the Rapid Manufacturing Laboratory of the Production Engineering Department of the Poznań University of Technology exports data from the STL mesh in the MeshLab program to a previously prepared template Excel file, which is connected to the autogenerating model.

In the MeshLab program, the STL grid of the patient's residual limb is located in the central part of the coordinate system so that the Z axis of the system is the imaginary axis of the arm.











The scan of the stump must be oriented with its inner part in the direction of the X axis ("up") in order to correctly generate the loosening holes and tissue compression pads (Figure 2).

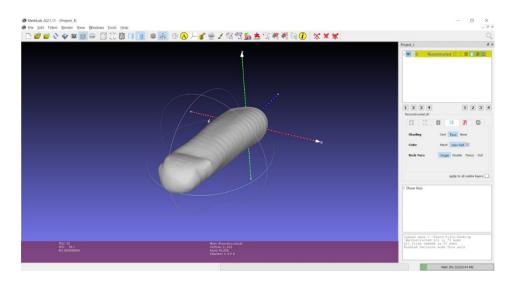


Figure 2 Correct orientation of the STL mesh in MeshLab

First, with the Offset from Plane command, six work planes (Figure 3) were created as offsets from the XY origin plane of the coordinate system (Figure 4). The value of the offsets of individual planes from the XY plane is defined by the user parameter P_n , where $n \in \langle 1:6 \rangle$ is the number of the plane.

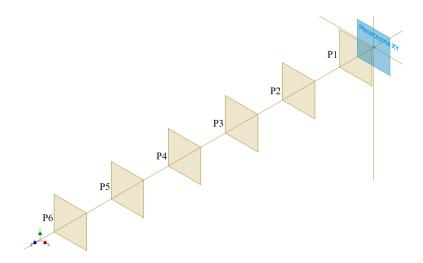


Figure 3 Construction planes defining cross-sections through the patient's vestigial limb











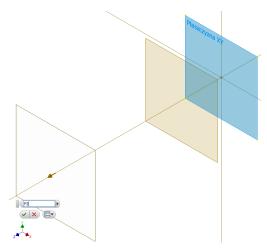


Figure 4 Generating a plane using the Offset from Plane function

The P1 plane marks the place of the first cross-section through the STL mesh of the patient's stump, and thus the edge of the prosthetic socket. The plane P6, on the other hand, marks the place of the last section through the distal part of the vestigial limb and defines the end of the socket. The positions of these two planes are determined in the special AutoMedPrint Limb Calibrator application provided by the team of the Virtual Design Laboratory of the Poznań University of Technology (Figure 5).

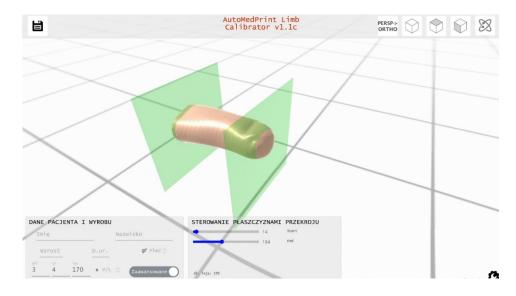


Figure 5 Determination of the extreme positions of the residual limb cross-sectional planes - the AutoMedPrint Limb Calibrator application











The algorithm fills an Excel workbook with data, thanks to the implemented rules, the model is loaded with information necessary to generate the model (e.g. the value of the offset between the planes, or the position of the next planes. The user parameters created at this stage were combined with the model parameters (Figure 6) in the dialog box Inventor Parameters.

| HŦ | d0 | Płaszczyzna konstrukcyjna1 | mm | P1 |
|----------|----|----------------------------|----|----|
| | d1 | Płaszczyzna konstrukcyjna2 | mm | P2 |
| . | d2 | Płaszczyzna konstrukcyjna3 | mm | P3 |
| | d3 | Płaszczyzna konstrukcyjna4 | mm | P4 |
| Ī | d4 | Płaszczyzna konstrukcyjna5 | mm | P5 |
| Ī | d5 | Płaszczyzna konstrukcyjna6 | mm | P6 |

Figure 6 Model parameters related to construction planes

The next step in constructing the prosthetic socket was to create six sketches on previously generated planes. Each sketch is a spline curve built from eight points specified by x and y coordinates. Initially, splines were drawn based on random points. After combining the model parameters with the user parameters from Excel, using the Update Local function, the coordinates of the spline building points were updated. As a result of the update, the outline that a single spline forms is the outline of a cross-section through the vestigial limb (Figure 7).

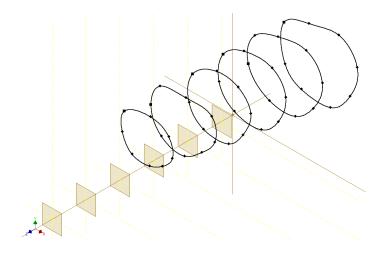


Figure 7 Six splines mapping the outline of cross-sections through the patient's vestigial limb

The data exported from one section in MeshLab are the x, y, z coordinates of the points forming the outline of the stump at the location of this section. The algorithm randomly selects











eight points with a specified spacing between them and completes the cells in the Excel spreadsheet (Figure 8). The x coordinates are specified by the user parameter x_{i-j} , where $i \in \langle 1:8 \rangle$ is the spline point number and $j \in \langle 1:6 \rangle$ is the sketch number.

| 8 | x1_1 | -36,03267 |
|----|------|-----------|
| 9 | y1_1 | 20,41032 |
| 10 | x2_1 | -10,21343 |
| 11 | y2_1 | 32,27849 |
| 12 | x3_1 | 20,57136 |
| 13 | y3_1 | 37,30608 |
| 14 | x4_1 | 39,542 |
| 15 | y4_1 | 17,76262 |
| 16 | x5_1 | 32,19633 |
| 17 | y5_1 | -11,46023 |
| 18 | x6_1 | 11,69784 |
| 19 | y6_1 | -31,69644 |
| 20 | x7_1 | -18,21643 |
| 21 | y7_1 | -30,42693 |
| 22 | x8_1 | -34,93382 |
| 23 | y8_1 | -16,15504 |
| | | |

Figure 8 The x, y coordinates of the spline building points, sketch #1

In the next step, using the Extrude from sketches function, six extrusions were created with a distance of each extrusion equal to 1 mm. Then, six work points were generated on the extruded faces using the Edge Loop Midpoint function (Figure 9).



Figure 9 Extrusions with work points











Then another six sketches were created on the back faces of the extrusions. A single sketch consists of projected cutting edges and three offsets from the outline of the reference geometry (Figure 10). The first offset determines the wall thickness of the socket taking into account the offset of the prosthetic socket surface from the surface of the residual limb. The second offset defines the offset of the inner socket wall from the residual limb. The last offset determines the thickness of the compression pads, taking into account the offset of the socket surface from the stump surface.

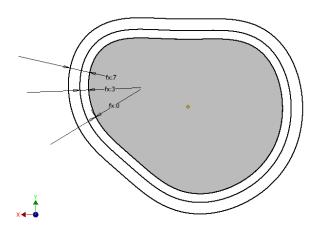


Figure 10 Three offsets from the section outline

After calculating the values of the offsets, applying them and using the loft function, a solid was obtained (Figure 11).

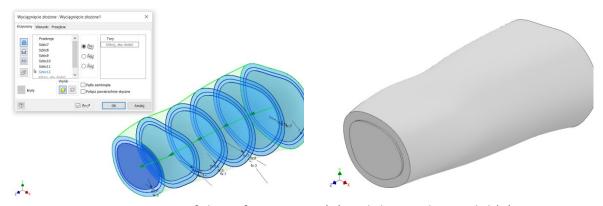


Figure 11 Execution of the Loft operation (A) and the resulting solid (B)











Then, by performing the Loft operation again, this time in Cutout mode, the inner part of the solid was cut out (Figure 12).

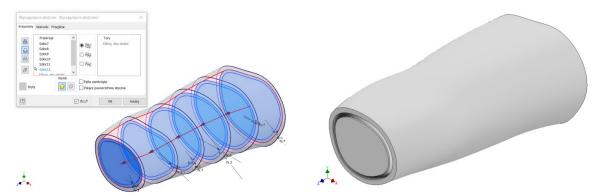


Figure 12 Execution of the Loft operation in Cutout mode (A) and the resulting solid (B)

At the last stage of generating the basic geometry of the prosthetic socket, its end was modeled. To do this, two Close Boundary operations were performed with a tangency condition assigned a parameter named boundary_close. As a result, two convex construction surfaces were generated, defined by the outer and inner edges of the geometry, respectively (Figure 13A). In addition, the Sculpture operation was performed, which resulted in generating a solid bounded by two surfaces of the envelope closure (Figure 13B).

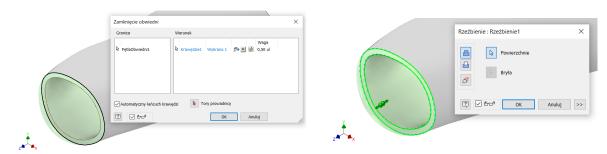


Figure 13 Perform a Close Boundary operation (A) and a Sculpture operation (B)

The next step was to model the geometry of the compression pads (the compression part of the socket) using the Loft operation in the New Solid mode, through previously created sketches. Then, a Loft operation was performed in Cutout mode based on the curves defining the thickness of the inserts (Figure 14A). The result was a second body with a wall thickness equal to that of the compression pads (Figure 14B).











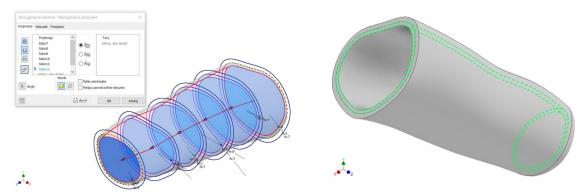


Figure 14 Execution of the Loft operation in Cutout mode (A) and the resulting solid (B)

In the next step, four holes were made to accommodate the tissue compressed by the inserts (relaxation part of the socket). For this purpose, two work planes were created using the Parallel to plane through point function, where Work Point 1 and the YZ and XZ planes were used as references in both cases. Four sketches were then created, with the reference points being two work points #1 and #6. Cuts were made in both solids using asymmetric Revolve operations in Cutout mode (Figure 15). Using the asymmetry mode gives you the ability to modify the size of the hole in two directions from the plane on which the sketch is located.

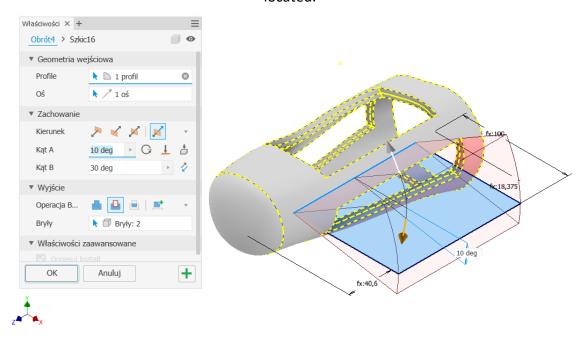


Figure 15 Making a hole using the Revolve operation











The dimensions that define the sketches are assigned user parameters - they are calculated using rules implemented in the Excel spreadsheet.

Then, two Extrude operations were performed in Cut-out mode, trimming the compression pads to the length of the hole on the inside of the socket. In the next step, roundings of the geometry of the inserts and holes were created. Then, using the Create Combination function, the two solids were joined together and the rest of the fillets were made. As a result, the finished socket geometry was obtained (Figure 16).

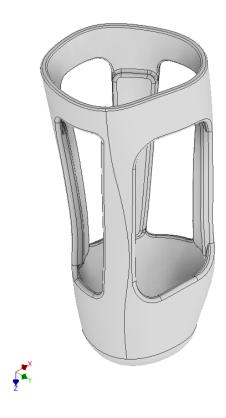


Figure 16 Modeled geometry of the prosthetic socket

The next step was to connect the CRS socket with the forearm. For this purpose, two solutions by making a version with universal mounting and the possibility of disabling the built-up bottom (Figure 17A) and with a version with recessed mounting (Figure 17B).

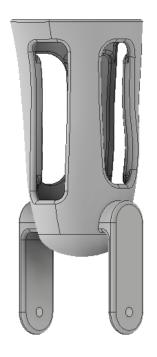












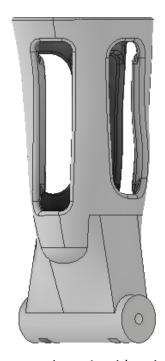


Figure 17 CRS sockets obtained as a result of analogous operations: A: with universal fastening; B: with flush mount

2.3.2 Forearm

The modular model of the prosthesis assumes the possibility of personalization and generating its modified variants. As part of this work, a model of the open forearm - dedicated to children and the closed forearm - for adults was presented. This is related to the load imposed by the user. The spatial form of the forearms is created by a complex extrusion, connecting two cross-sections - the first showing a rectangle with rounded corners and the second - its offset version, defined by the offset parameter. You can manipulate the parameter while keeping the width of the first sketch constant. Therefore, the parameter dimension_j was also introduced to the geometry of the forearms, matching it to the designed adapters. However, the offset parameter (Figure 18) was retained, enabling the automatic generation of a second cross-section proportional to the wrist, distanced by the length of the Forearm determined on the basis of the spatial scan (also the output parameter from the original supply sheet).









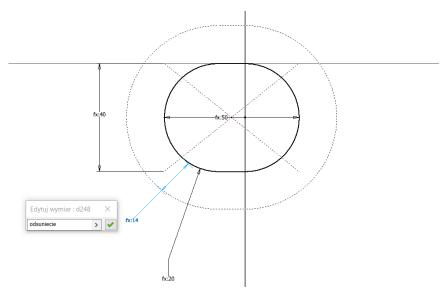


Figure 18 Base for forearm geometry

The introduction of a universal dimension then made it possible to associate other design features with it, such as e.g. joint spacing. Parameters describing other geometrical features, such as an indentation in the bottom wall, were also combined to proportionally change their size as the length of the component changes (Figure 20A). The dimension of additional extrusions used for assembly with a prosthetic socket was also increased, changing the radius of the element from 9 to 12 mm (Figure 20B) and the dimension of the diameter of the mounting hole was parameterized (, currently equal to 5.2 mm).

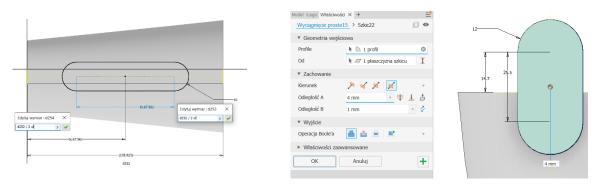


Figure 19 A: Relationship between the length of the Forearm and the dimensions of the notch in the bottom wall. B: Widening of the forearm assembly parts











Then, three more variants of the Forearm were made, taking into account the assembly of adapters. They include a forearm in the classic open version with an appropriate tip, a forearm with a structure closed from the outside but empty inside (eliminating the operation of cutting in the upper and lower walls) and a completely built-up body.

The indentation in the tip dedicated to the assembly of the adapter was made at the initial stage of modeling the forearms, just before the use of the shell operation hollowing out the element from the inside. On the surface described by the base sketch, another one was added, on which the parameterized sketch of the external frame of the adapter was mapped. Then, it was moved away by 0.5 mm, designing the necessary clearance between the components, and a cutout was made in the solid at a distance of 22 mm, i.e. to the height of the adapter (Figure 21).

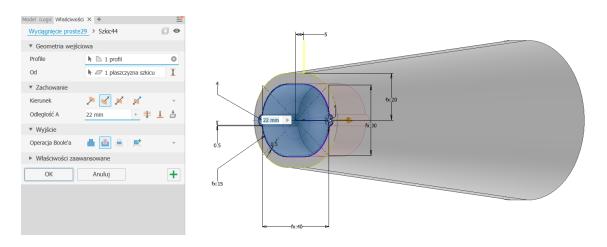


Figure 20 Designing geometry dedicated to the connection with the adapter - a cutout in the base solid

Further operations were performed at the end of modeling - a hole was designed for the convex part of the adapter, keeping 1 mm of clearance from the top and sides of the tab, a locking hole was made in the surface of the element and a widened indentation in the top









wall, which provides additional space for the protruding part of the thermoplastic fiber fixing the smaller element inside the adapter.

These operations made it possible to obtain a matching tip to the adapter introduced at the start. Similar steps were then performed for the closed and fully closed forearm. The first of the built-up forearms has retained the form of a classic component. However, the operation of making cuts along the upper structure and in the lower part of the element was eliminated from its construction (Figure 22).

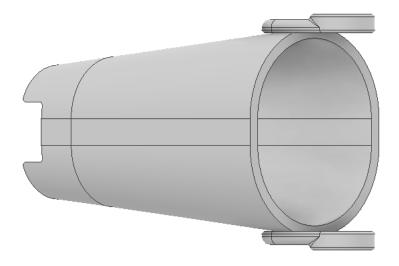


Figure 21 Closed forearm form

2.3.3 End effector

A C-handle was proposed as the effector, based on a simple horseshoe-shaped sketch (Figure 22).

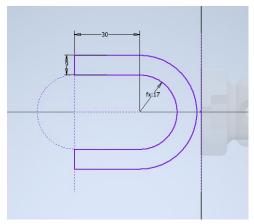












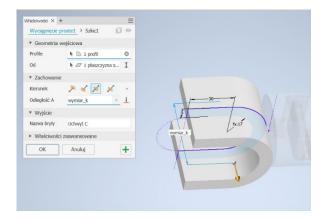


Figure 22 Start modeling the effector: A: sketch; B: straight pull out

An opening was then created to allow access to the mounting hardware of the adapter connecting the handle to the forearm (Figure 23).

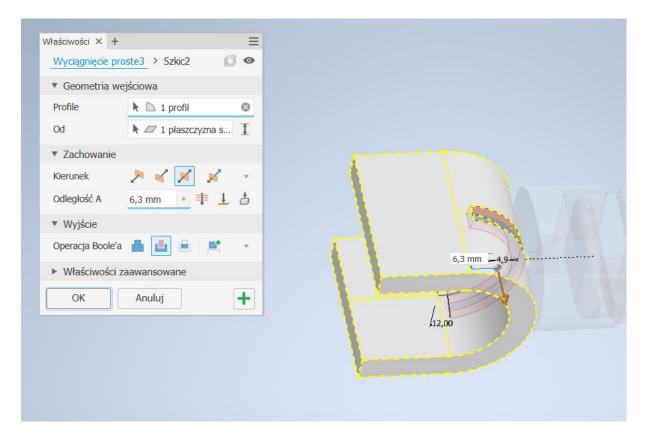


Figure 23 Opening for access to connecting elements



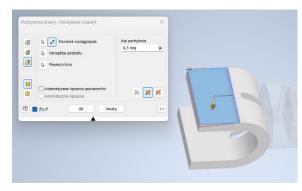








The next stage of work was to tilt the walls and round all sharp edges (Figure 24).



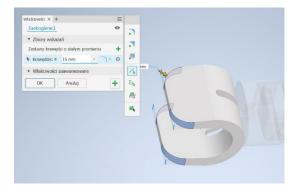


Figure 24 Successive stages of the formation of the effector: A: inclination of the walls,

B: rounding of the walls

The last stage was to model the element connecting the handle with the forearm using the extrude function on a previously prepared sketch (Figure 25).

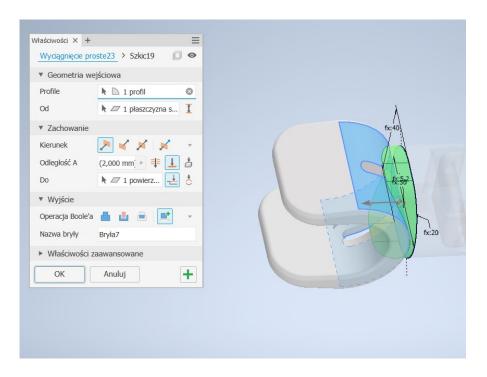


Figure 25 Connecting element to the wrist (extrude a previously prepared sketch)









Depending on the application, various effectors have been prepared, which, thanks to parameterization, form a coherent whole with other components, enabling each time tailored construction variants.

2.4 Final version of bicycle prosthesis

The modular prosthesis was generated using an generative (intelligent) model prepared for pediatric cases (Figure 26). The resulting model had to be adapted to the requirements of an adult user.

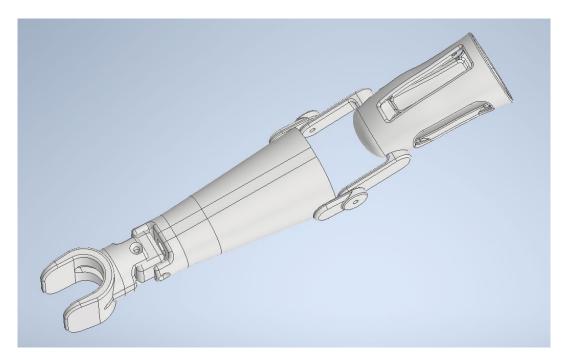


Figure 26 The effect of work of intelligent model - bicycle prosthesis for a child

First, the model was adjusted to the adult patient by 3D scanning and using functionalities of the intelligent model to re-create the geometry. Resulting prosthesis was 3D printed, assembled and tested by the patient (Figure 27).











Figure 27 Prosthesis made for a selected adult patient – test with the bicycle

In the course of numerous tests and subsequent design iterations, the following modifications have been introduced:

- The CRS socket was modified as a result of removing the movable connection in the elbow joint. It was connected to the forearm rigidly due to too much load in the case of an adult - the proposed movable connection used in the case of children's prostheses was breaking.
- The mounting plane was moved away from the tip of the socket to a properly selected distance. A circular sketch was made on the plane with dimensions to match the forearm, and then a loft operation was performed between the assembly plane and the selected socket section to achieve a smooth transition between the solids. These operations were performed before soft tissue cuts in the socket structure, because the











solid reached higher than the planned relaxation holes. Finally, mounting hardware was added to allow connection to the forearm (Figure 28).

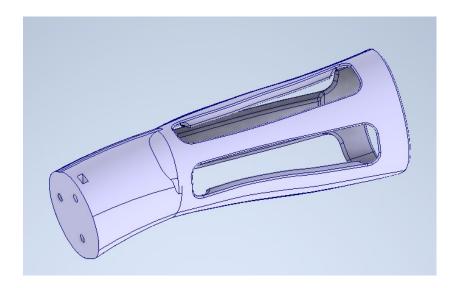
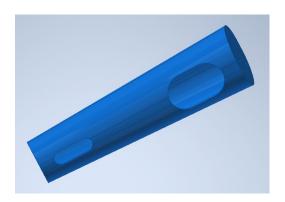


Figure 28 The final form of the CRS socket for an adult adapted to cycling

 Forearm - the model has been changed as a result of abandoning the movable joint in the elbow joint. In addition, its termination was modeled by using the function Close envelope with tangency condition. Finally, five mounting holes and two access holes were added (Figure 29).



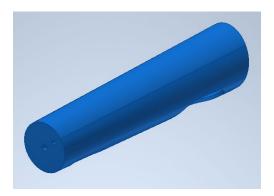


Figure 29 The final form of the forearm for an adult adapted to cycling



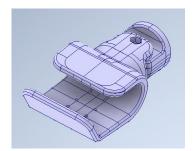








• The C-handle has been modified by extending the jaws and narrowing the distance between them. These changes were introduced after listening to Mr. Maciej's comments - they increased the stability and comfort of cycling. In addition, the connection used in the wrist was abandoned - the lack of a joint resulted in an increase in stiffness with the simultaneous impossibility of rotation. This was possible after adjusting the angles for a given patient and his bike.



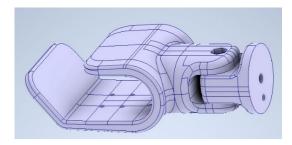


Figure 30 The final form of the C handle for an adult adapted to cycling

Figure 31 presents a complete model of the prosthesis prepared for an adult and adapted for cycling.

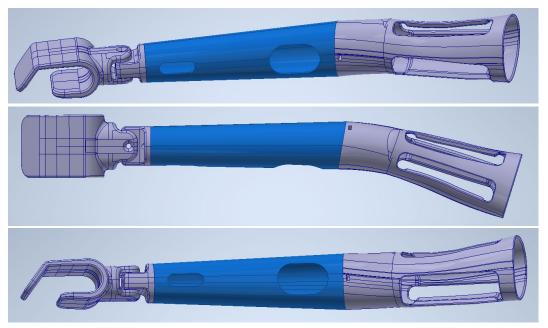


Figure 31 The final model of an adult bicycle prosthesis. View: A: Isometric; B: from above; B: from the side











- 2.5 Design of electronic part of the biomechatronic prosthesis
- 2.5.1 Main concept of the mechatronic prosthesis

The aim of the work was to modify the hand prosthesis in order to create a biomechatronic device, used by human, with monitoring of activities performed in the prosthesis (mostly cycling or similar activities). Main aim was placing an electronic measuring system in the prosthesis, thanks to which it would be possible to determine its operating properties. The detailed purposes of the built electronic system were to:

- measurement of the orientation of the upper limb prosthesis in space,
- measurement of the force exerted in the wrist,
- saving data on the SD card.

The device consisted of the following components:

- microcontroller module (Arduino NANO),
- force sensor measuring amplifier module (HX711 with force sensor up to 200N),
- inertial sensor module (BOSCH BNO055),
- SD card module,
- power source (a USB connected powerbank).

The components were selected to fulfil their role in the simplest possible manner, ensuring robust operation, steady and stable communication, as well as maintaining as low price as possible (as the whole prosthesis is also a low-cost project). The schematic diagram of the designed device is shown in the Figure 32.









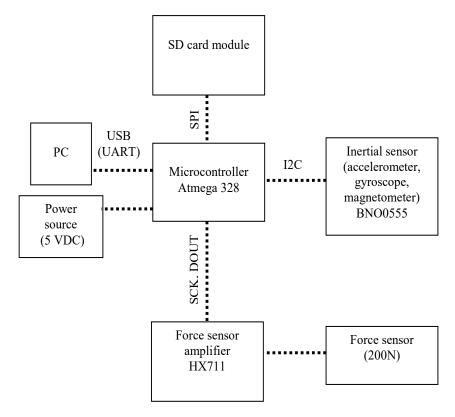


Figure 32 The schematic diagram of the electronic part of the prosthesis

2.5.2 Design modifications in biomechatronic prosthesis

The final mechanical version of the prosthesis was first manufactured and tested by the patient to confirm its usefulness. Then, another set of requirements were introduced – namely, to be able to fit the electronics of the prosthesis inside it, in a manner allowing steady riding on a bicycle or similar device, without risk of disconnecting or otherwise damaging the components, as well as not making them disturb the patient during the activities.

The following main changes have been introduced to the design:

 the forearm was modified to enable mounting of the microcontroller, inertial sensor and SD card module inside cavities of the forearm – insets were created with holes, for self-tapping purposes (Figure 33)











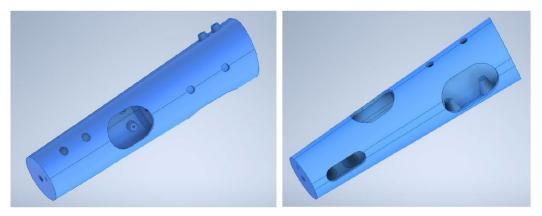


Figure 33 Modified forearm – visible mounting places for electronic components

- at the joint of forearm and CRS socket, insets were added for mounting of the force sensor (beam) – the place (elbow) was selected to easily detect the torques and forces during the bicycle ride
- a number of assembly holes and cable feedthroughs were added to enable unproblematic assembly of the electronic part inside the prosthesis.

Final version of the CAD model of the prosthesis is shown in Figure 34.

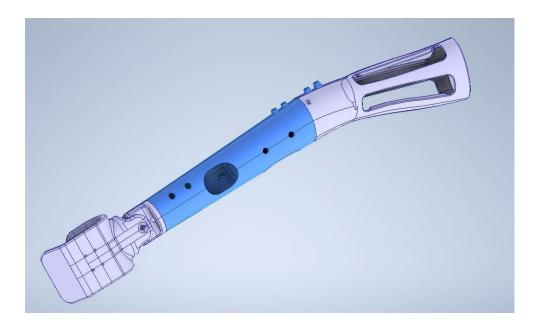


Figure 34 Final CAD model of the biomechatronic bicycle prosthesis











3 Summary

In this toolkit, it was shown how a modular model of a low-cost 3D printed bicycle prosthesis can be designed and then converted into a simple biomechatronic device, equipped with sensors for biometrics of the bicycle ride activity. The toolkit is a part of the set of instructions, focused on the prosthesis model. The resulting model was 3D printed in further steps and then assembled, tested in laboratory conditions and then in real conditions, with the patient – this is described in other toolkits of the EMERALD project.

Literature

- Górski, F., Wichniarek, R., Kuczko, W., Żukowska, M., Rybarczyk, J., & Lulkiewicz, M. (2022). Evaluation of a Prototype System of Automated Design and Rapid Manufacturing of Orthopaedic Supplies. In Advances in Manufacturing III: Volume 5-Biomedical Engineering: Research and Technology Innovations, Industry 4.0 (pp. 1-15). Cham: Springer International Publishing.
- 2. Górski, F., Wichniarek, R., Kuczko, W., & Żukowska, M. (2021). Study on properties of automatically designed 3d-printed customized prosthetic sockets. Materials, 14(18), 5240.
- 3. Komorowska O., 2022, Automation of design of modular upper limb prosthesis, Master's Thesis (supervision: Górski F.), Poznan University of Technology
- 4. Słupińska S., 2021, Automation of design of low-cost upper limb cosmetic prostheses, Master's Thesis (supervision: Górski F.), Poznan University of Technology









EMERALD

The Education, Scholarships, Apprenticeships and Youth Entrepreneurship

EUROPEAN NETWORK FOR 3D PRINTING OF BIOMIMETIC

MECHATRONIC SYSTEMS

E-toolkit – Computer Aided Engineering (CAE)

| Project Title | European network for 3D printing of biomimetic mechatronic systems 21-COP-0019 | |
|------------------|---|--|
| Output | IO2 – E-toolkit for teaching purposes, basic knowledge about realizing biomimetic mechatronic systems | |
| Module | Computer Aided Engineering (CAE) | |
| Date of Delivery | y July 2022 | |
| Authors | Dan-Sorin COMŞA, TUCN | |
| Version | Final (January 16, 2023) | |









Contents

| 1. | Introduction | 3 |
|----|---|----|
| 2. | Preparation of the finite element model | 6 |
| 3. | Interpretation of the numerical results | 29 |
| 4. | Suggestions for individual work | 37 |
| Do | forences | 20 |

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2



1. Introduction

The objective of this application is to evaluate the strength characteristics of an upper-limb prosthesis (Fig. 1) by simulating a distal tensile test with the finite element analysis (FEA) module SolidWorks Simulation [WWW2022b] included in the SolidWorks CAD package [WWW2022a]. The principle of the test is shown in Figure 2. As one may notice, the prosthesis is subjected to a distal traction load after being firmly attached to a rigid support that fits inner surfaces of the upper arm. The traction load gradually increases from 0 (zero) to 750 N.

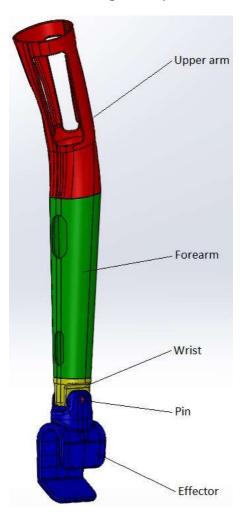


Figure 1: 3D model of the upper-limb prosthesis













Figure 2: Principle of the distal tensile test simulated for evaluating the strength characteristics of the upper-limb prosthesis (red surfaces – regions where the upper arm is firmly attached to a rigid support; blue surface – support of the traction load)











The following hypotheses are adopted when preparing the finite element model of the tensile test:

- The prosthesis components are made of PETG exhibiting an isotropic linear elastic behavior. Table 1 lists the physical and mechanical properties of this material that are relevant for the finite element model of the tensile test.
- The prosthesis components are bonded together along their contact surfaces.

Table 1: Physical and mechanical properties of PETG [Kan2020]

| Mass density | Elastic modulus | Poisson's ratio | Yield strength |
|-----------------------------|-----------------|-----------------|----------------|
| ρ [kg/m ³] | <i>E</i> [MPa] | v [-] | Y [MPa] |
| 1270 | 1660 | 0.419 | 30.3 |

The input files needed for preparing the finite element model of the tensile test are stored in the folder *Upper-limb prosthesis FEA*:

Upper arm.SLDPRT – 3D model of the upper arm (Fig. 1)
 Forearm.SLDPRT – 3D model of the forearm (Fig. 1)
 Wrist.SLDPRT – 3D model of the wrist (Fig. 1)
 Effector.SLDPRT – 3D model of the effector (Fig. 1)
 Pin.SLDPRT – 3D model of the pin (Fig. 1)

Upper-limb prosthesis.SLDASM – 3D model of the prosthesis (Fig. 1)

EMERALD CAE Materials.sldmat – custom library storing the physical and mechanical properties of PETG listed in Table 1.

The selection set *Selection-Set1(10) Upper arm - Fixed* (defined in the file *Upper-limb prosthesis.SLDASM*) collects the surfaces where the upper arm is firmly attached to the rigid support.

The displacement (deflection), force and stress quantities manipulated by the FEA model are expressed using the following measurement units: displacement (deflection) – millimeter [mm]; force – Newton [N]; stress – megapascal [MPa] (1 MPa = 1 N/mm²).

The next sections of this documentation describe the preparation of the FEA model and the interpretation of the numerical results.











2. Preparation of the finite element model

The FEA model of the tensile test (Fig. 2) is developed by performing the following steps:

a) Open the Upper-limb prosthesis.SLDASM model in SolidWorks (Fig. 3).

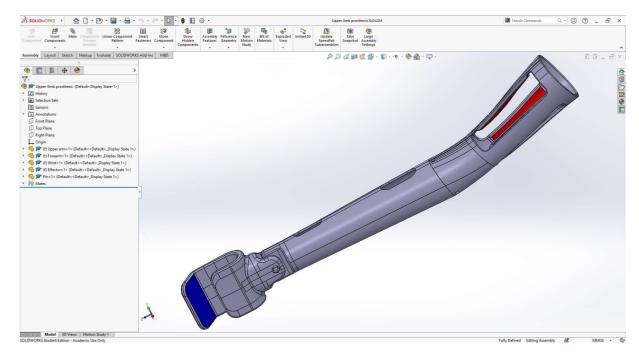


Figure 3: Upper-limb prosthesis.SLDASM model open in SolidWorks

- b) Activate the SolidWorks Simulation module by accessing the "SOLIDWORKS Add-Ins" tab of the "Command Manager" toolbar (Fig. 4) and pressing the "SOLIDWORKS Simulation" button (Fig. 5). Consequently, the "Simulation" tab is included in the "Command Manager" toolbar (Fig. 6).
- c) Change some working parameters of the SolidWorks Simulation module by accessing the "Simulation" menu and selecting the "Options..." command (Fig. 7). Consequently, the "System Options General" window is displayed. In the "Default Options" panel, select the SI (MKS) unit system, then change the following measurement units: length/displacement [mm] and pressure/stress [N/mm²] (Fig. 8).













Figure 4: "SOLIDWORKS Add-Ins" tab in the "Command Manager" toolbar



Figure 5: "SOLIDWORKS Simulation" button in the "SOLIDWORKS Add-Ins" toolbar



Figure 6: "Simulation" tab included in the "Command Manager" toolbar after the activation of the SolidWorks Simulation module

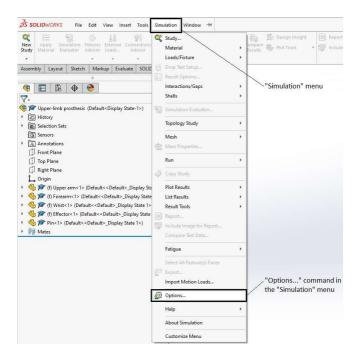


Figure 7: "Options..." command in the "Simulation" menu











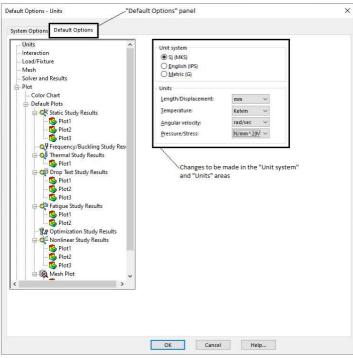


Figure 8: Changes to be made in the "Default Options" panel of the "System Options – General" window

- d) Add the folder *Upper-limb prosthesis FEA* to the list of places where SolidWorks looks for material libraries by accessing the "Tools" menu and selecting the "Options..." command (Fig. 9). Consequently, the "System Options General" window is displayed. In the "System Options" panel, select the "File Locations" entry (Fig. 10). Unroll the "Show folders for:" drop-down list and select the "Material Databases" item (Fig. 11). After pressing the "Add..." button (Fig. 12), the "Select Folder" window is displayed on the screen (Fig. 13). Look for the folder *Upper-limb prosthesis FEA*, select it and press the "Select Folder" button placed at the bottom of the "Select Folder" window (Fig. 13). Press the "OK" buttonplaced at the bottom of the "System Options General" window (Fig. 14).
- e) Enter the "Simulation" toolbar and press the "New Study" button (Fig. 15) to create a FEA model having the following characteristics (Fig. 16):
 - name of the FEA model: "Static 1"
 - type of the FEA model: "Static".

Press the "OK" button placed at the upper-left corner of the "Study" window (Fig. 16).











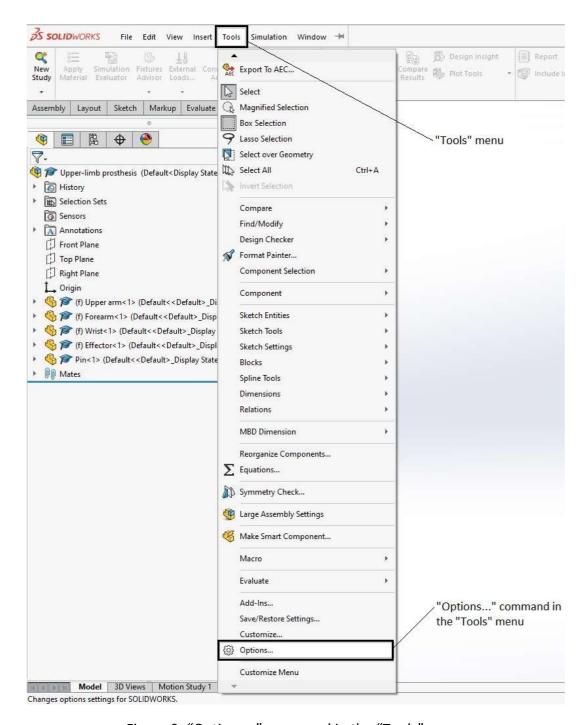


Figure 9: "Options..." command in the "Tools" menu











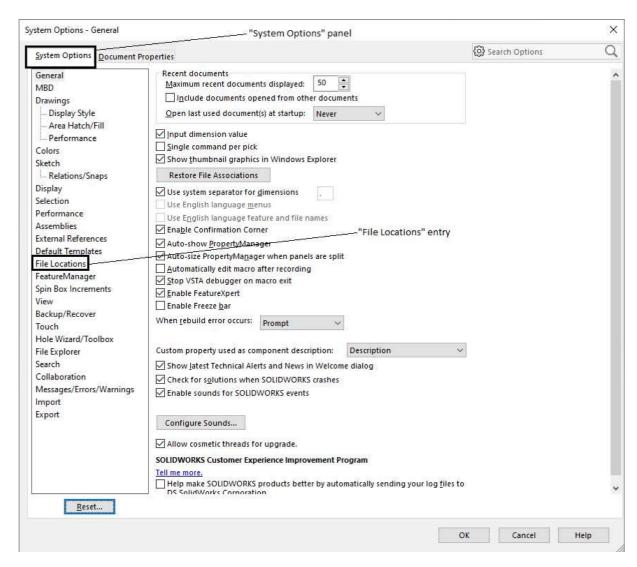


Figure 10: "File Locations" entry in the "System Options" panel of the "System Options – General" window











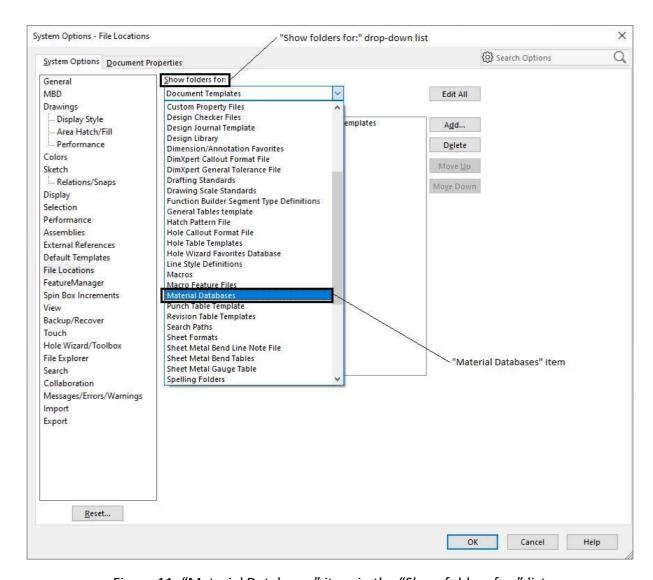


Figure 11: "Material Databases" item in the "Show folders for:" list











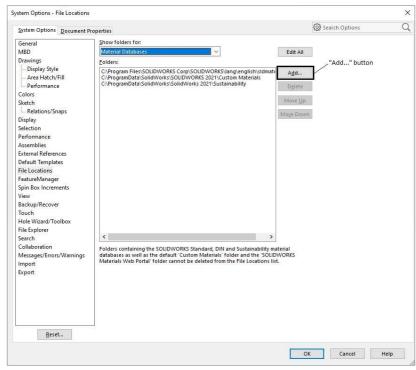


Figure 12: "Add..." button to be pressed for modifying the list of places where SolidWorks looks for material libraries

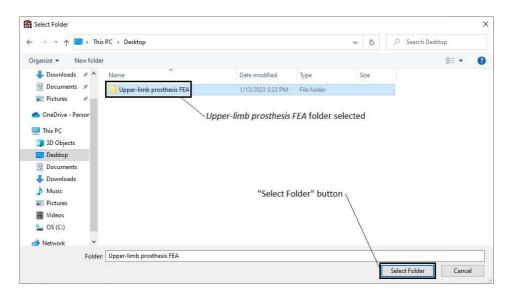


Figure 13: Selecting the folder *Upper-limb prosthesis FEA* for being added to the list of places where SolidWorks looks for material libraries











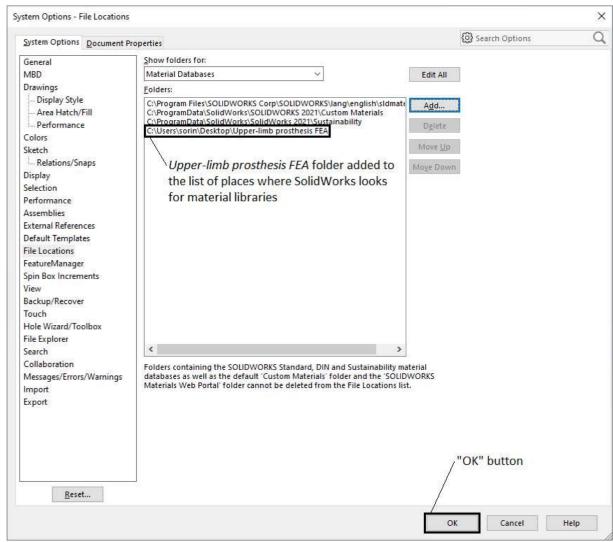


Figure 14: Folder *Upper-limb prosthesis FEA* included in the list of places where SolidWorks looks for material libraries



Figure 15: Creation of a new FEA model











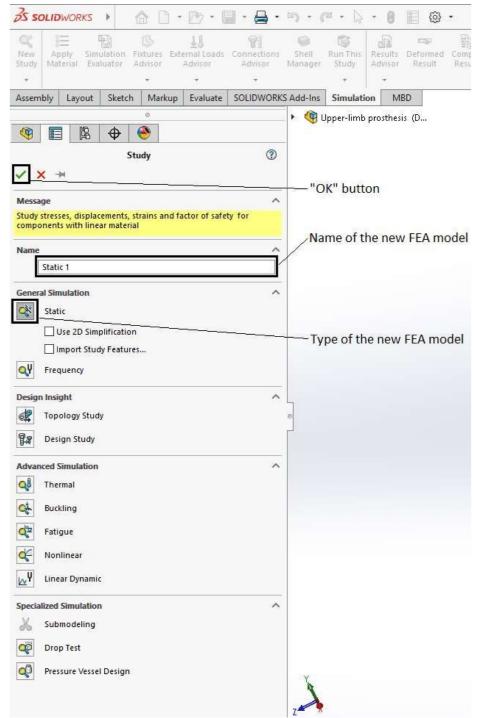


Figure 16: Defining the name and type of the new FEA model









f) Press the right button of the mouse on the "Parts" entry of the FEA tree and select the "Apply Material to All..." command from the drop-down menu to define the material properties of the prosthesis components (Fig. 17). Consequently, the "Material" window is displayed (Fig. 18). In that window, minimize the "SOLIDWORKS Materials" library, unroll the "EMERALD CAE Materials" library, unroll the "Plastics" category, select the "PETG" material, then press the buttons "Apply" and "Close" placed at the bottom of the "Material" window.

Note: The yield strength Y = 30.3 MPa (see the PETG material data listed in Table 1 and Figure 18) defines the upper limit of the von Mises equivalent stress that can be supported by the prosthesis components.

g) Do not change the option "Global Interaction (-Bonded-Meshed Independently-)" activated by default under the "Connections" and "Component Interactions" entries of the FEA tree (Fig. 19). This option is consistent with the hypotheses formulated in §1.

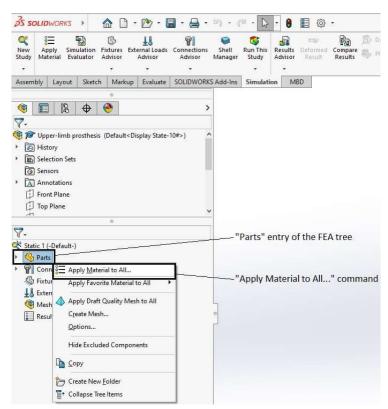


Figure 17: Defining the material properties of the prosthesis components











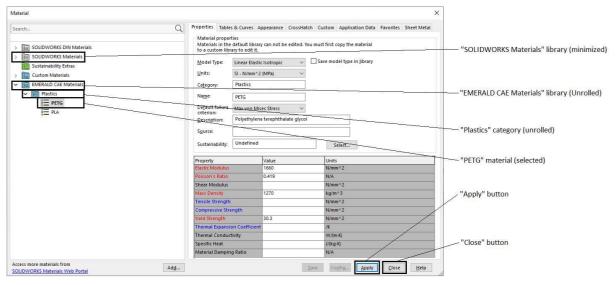


Figure 18: Associating the PETG material to the prosthesis components

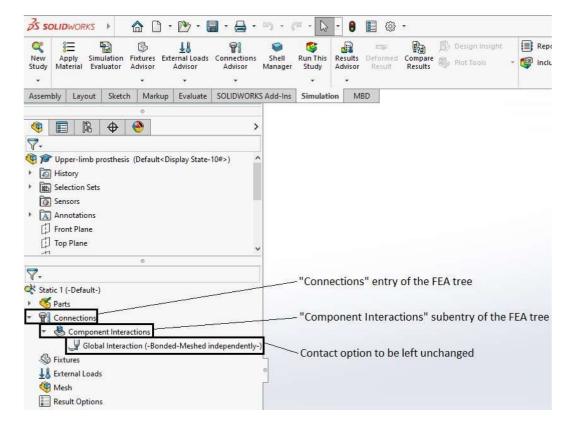


Figure 19: Contact option activated by default in the FEA tree (to be left unchanged)











- h) Press the right button of the mouse on the "Fixtures" entry of the FEA tree and select the "Fixed Geometry..." command in the drop-down menu (Fig. 20). Perform the following actions in the "Fixture" dialogue box to define a full locking boundary condition on some inner surfaces of the upper arm (Fig. 21):
 - Press the left button of the mouse in the "Faces, Edges, Vertices for Fixture" selection box of the "Fixture" dialogue box
 - Unroll the assembly tree placed at the upper-left corner of the SolidWorks graphics area
 - Unroll the "Selection Sets" entry of the assembly tree
 - Select "Selection-Set1(10) Upper arm Fixed" in the assembly tree
 - Press the "OK" button of the "Fixture" dialogue box.

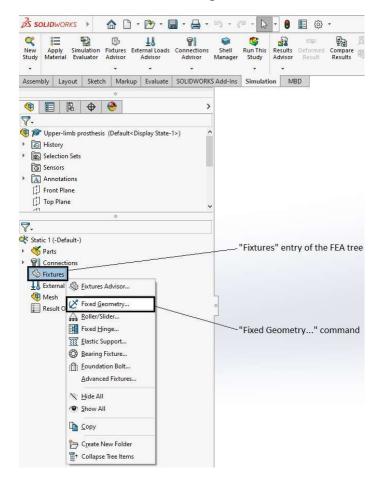


Figure 20: Defining full locking boundary conditions











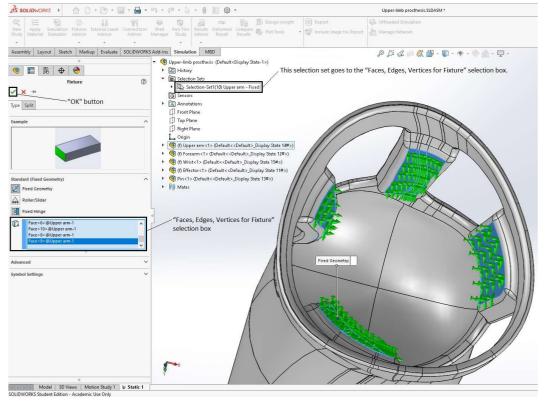


Figure 21: Full locking boundary conditions defined on some inner surfaces of the upper arm

- i) Press the right button of the mouse on the "External Loads" entry of the FEA tree and select the "Force..." command in the drop-down menu (Fig. 22). Perform the following actions in the "Force/Torque" dialogue box to define the distal traction load that acts on the prosthesis (Fig. 23):
 - Activate the "Selected direction" radio button
 - Press the left button of the mouse in the "Faces, Edges, Vertices, Reference Points for Force" selection box
 - Select the blue surface of the prosthesis effector in the SolidWorks graphics area
 - Press the left button of the mouse in the "Face, Edge, Plane for Direction" selection box
 - Unroll the assembly tree placed at the upper-left corner of the SolidWorks graphics area











- Select "Front Plane" in the assembly tree
- Press the "Normal to Plane" button in the "Force" region of the "Force/Torque" dialogue box
- Do not change the force value specified by default (1 N) in the "Normal to Plane" input box
- Press the "OK" button of the "Force/Torque" dialogue box.

Note: The actual values of the traction force are defined in step (k) as load cases.

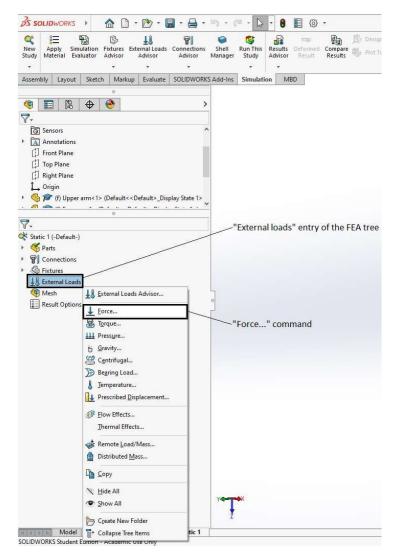


Figure 22: Defining a force-type boundary condition











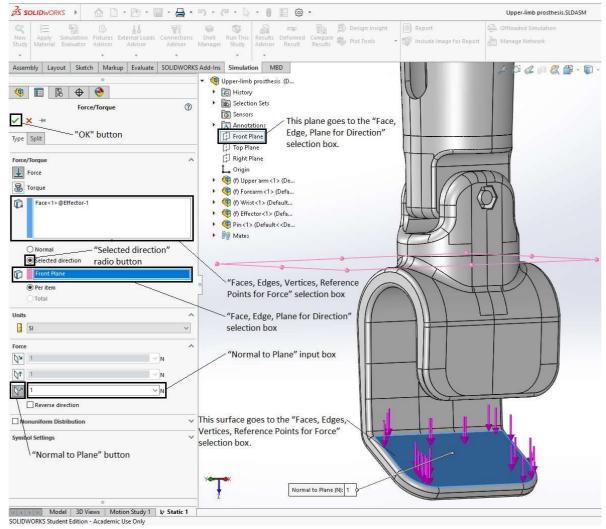


Figure 23: Defining the distal traction load that acts on the prosthesis

- j) Press the right button of the mouse on the "Mesh" entry of the FEA tree and select the "Create Mesh..." command in the drop-down menu (Fig. 24). Perform the following actions in the "Mesh" dialogue box to generate the finite element mesh (Fig. 25):
 - Move the "Mesh Factor" cursor to the "Fine" position
 - Press the "OK" button of the "Mesh" dialogue box.

Note: The finite element mesh generated by SolidWorks Simulation is shown in Figure 26.











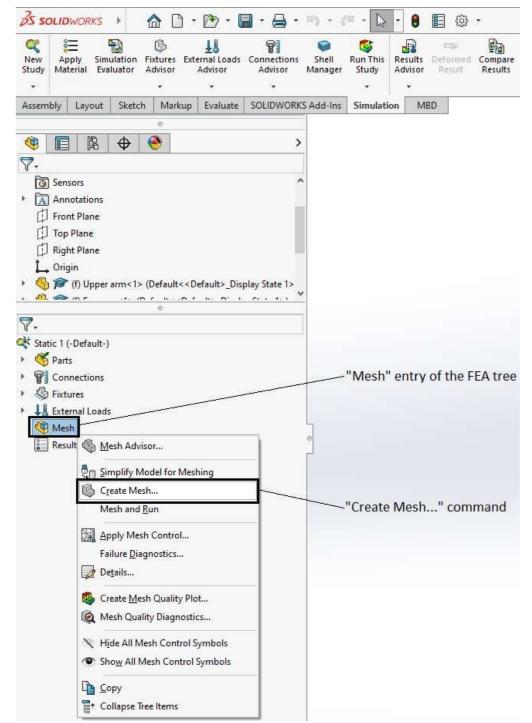


Figure 24: Initiating the generation of the finite element mesh











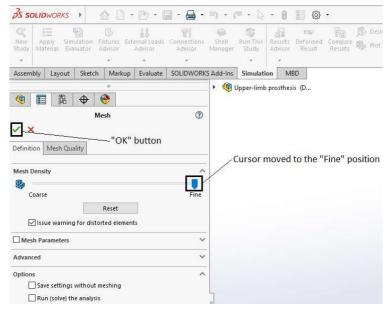


Figure 25: Defining the control parameters of the finite element mesh

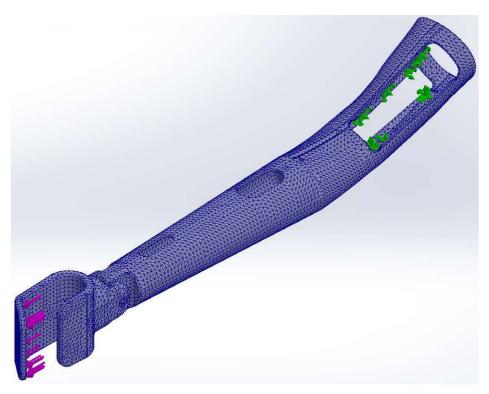


Figure 26: Finite element mesh generated by SolidWorks Simulation











- k) Press the right button of the mouse on the root of the FEA tree and select the "Load Case Manager" command in the drop-down menu (Fig. 27). Consequently, the "Load Case View" tab is displayed at the bottom of the SolidWorks graphics area (Fig. 28). Perform the following actions in that tab to define the actual values of the traction load that acts on the prosthesis:
 - Press the left button of the mouse in the box labeled "+ Click here to add a primary load case" to define the first load case (Fig. 29)
 - Replace the "Suppress" status of the "Force-1" cell with 150 (Newton) i.e., the actual value of the pressure corresponding to "Load Case 1" (Fig. 29)
 - Press the left button of the mouse in the box labeled "+ Click here to add a primary load case" to define the second load case (Fig. 29)
 - Replace the "Suppress" status of the "Force-1" cell with 300 (Newton) i.e., the actual value of the pressure corresponding to "Load Case 2" (Fig. 30)
 - Proceed in the same manner to define "Load Case 3": 450 N, "Load Case 4": 600 N, and "Load Case 5": 750 N (Fig. 31)
 - Press the left button of the mouse in the box labeled "+ Click here to add a sensor to track a result" (Fig. 31)
 - Select the "+ Add Sensor..." command in the drop-down list displayed at the bottom of the "Load Case View" tab (Fig. 32)
 - Perform the following actions in the "Sensor" dialogue box to define a sensor for tracking the maximum value of the von Mises equivalent stress at the level of the entire FEA model (Fig. 33):
 - Select the option "Stress" from the "Results" drop-down list
 - Select the option "VON: von Mises Stress" from the "Component" drop-down list
 - Select the option "N/mm^2 (MPa)" from the "Units" drop-down list
 - o Press the "OK" button placed at the upper-left corner of the "Sensor" dialogue
 - Come back to the "Load Case View" tab and press again the left button of the mouse in the box labeled "+ Click here to add a sensor to track a result" (Fig. 34)
 - Select the "+ Add Sensor..." command in the drop-down list displayed at the bottom of the "Load Case View" tab (Fig. 34)
 - Perform the following actions in the "Sensor" dialogue box to define a new sensor for tracking the maximum deflection at the level of the entire FEA model (Fig. 35):











- Select the option "Displacement" from the "Results" drop-down list
- Select the option "URES: Resultant Displacement" from the "Component" drop-down list
- Select the option "mm" from the "Units" drop-down list
- o Press the "OK" button placed at the upper-left corner of the "Sensor" dialogue.

At this stage, the finite element model of the tensile test is prepared and transferred to the SolidWorks Simulation solver by pressing the "Run" button of the "Load Case View" tab (Fig. 36). The numerical results generated by the solver are interpreted in the next section.

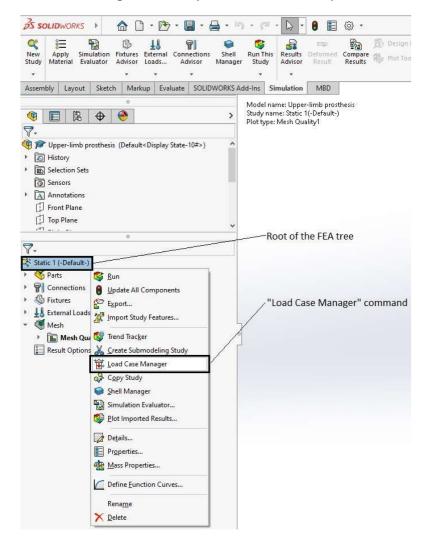


Figure 27: Accessing the Load Case Manager











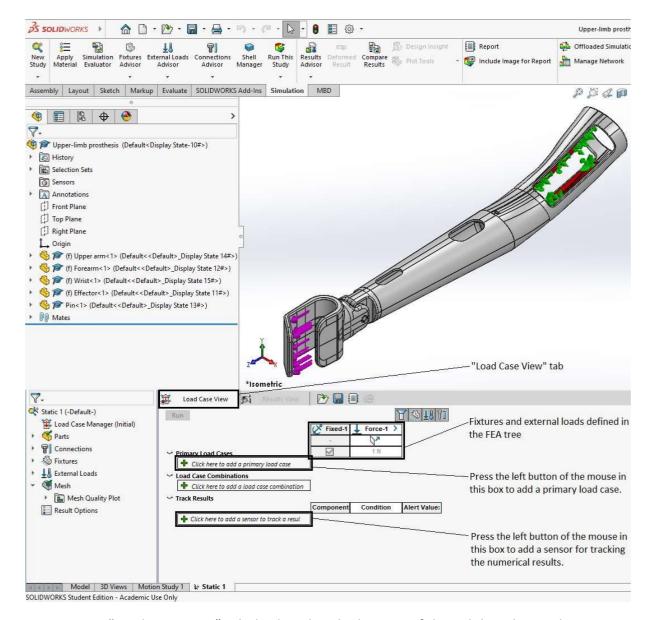


Figure 28: "Load Case View" tab displayed at the bottom of the SolidWorks graphics area











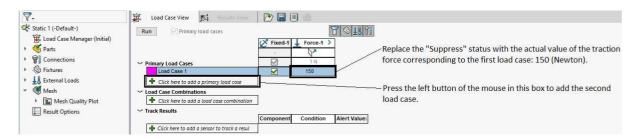


Figure 29: Defining the first load case (traction force of 150 N)

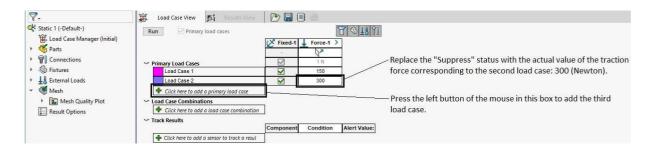


Figure 30: Defining the second load case (traction force of 300 N)

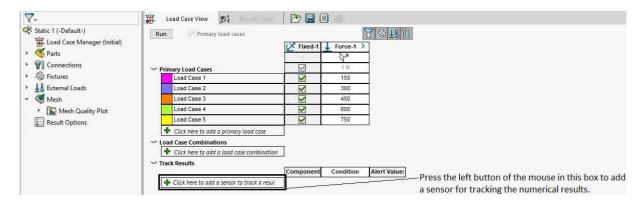


Figure 31: Actual values of the traction force defined as load cases











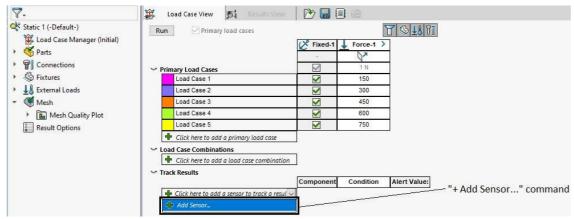


Figure 32: Initiating the definition of a sensor for tracking the numerical results

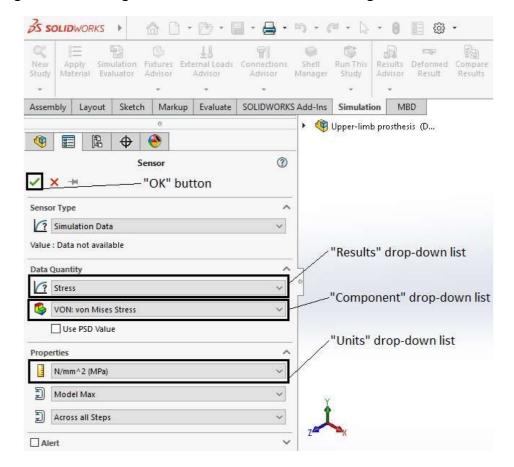


Figure 33: Definition of a sensor for tracking the maximum value of the von Mises equivalent stress at the level of the entire FEA model











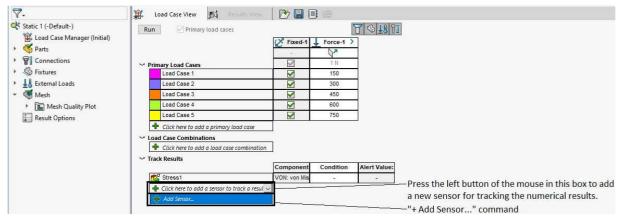


Figure 34: Initiating the definition of a new sensor for tracking the numerical results

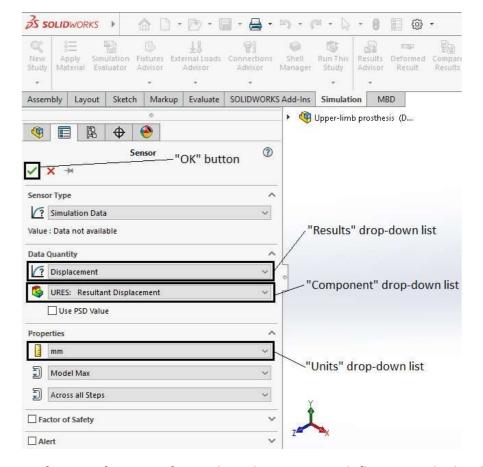


Figure 35: Definition of a sensor for tracking the maximum deflection at the level of the entire FEA model











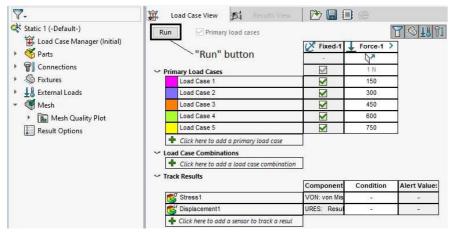


Figure 36: Transferring the finite element model to the SolidWorks Simulation solver

3. Interpretation of the numerical results

As soon as the solver finishes its job, the control is transferred to the "Results View" tab which is displayed at the bottom of the graphics area. At the same time, a color map showing the distribution of the von Mises equivalent stress at the level of the entire assembly appears on the screen (Fig. 37). This distribution corresponds to the first load case. The user can explore the other load cases by selecting them with the left button of the mouse in the first column of the "Primary Load Cases" table placed at the bottom of the "Results View" tab (see Figure 37, as well as the examples shown in Figures 38 and 39).

Perform the following actions to display the distribution of the deflection at the level of the entire assembly:

- a) Press the right button of the mouse on the item "Displacement1 (-Res disp-)" under the "Load Case Results" entry of the FEA tree, and select the "Show" command in the drop-down menu to examine the distribution of the deflection (Fig. 40)
- b) Examine the distribution of the deflection associated to different load cases by selecting them with the left button of the mouse in the first column of the "Primary Load Cases" table placed at the bottom of the "Results View" tab (see the examples shown in Figures 41 and 42).











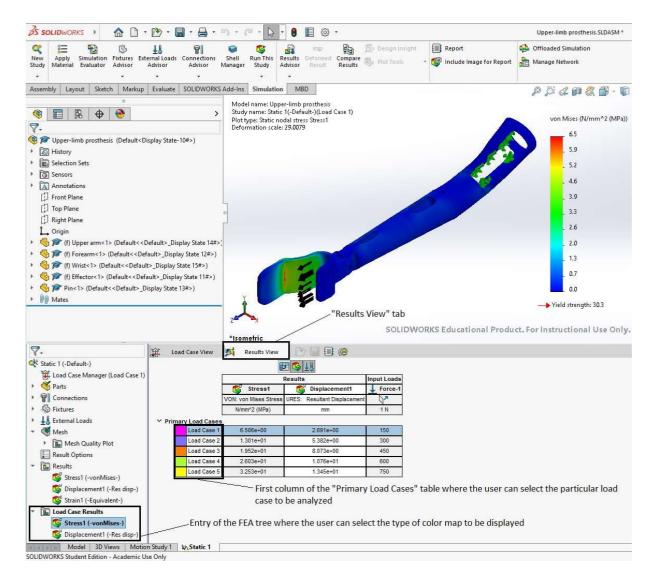


Figure 37: Analyzing the numerical results associated to different load cases with the help of the "Results View" tab and the "Load Case Results" entry of the FEA tree











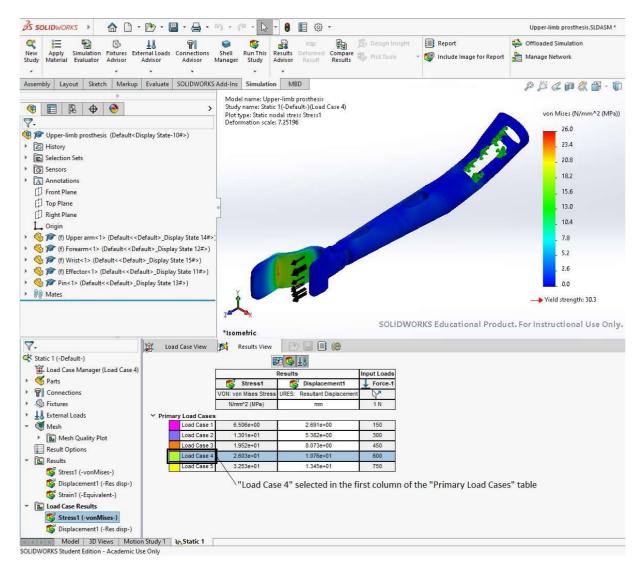


Figure 38: Color map showing the distribution of the von Mises equivalent stress at the level of the entire assembly (fourth load case: traction force of 600 N)











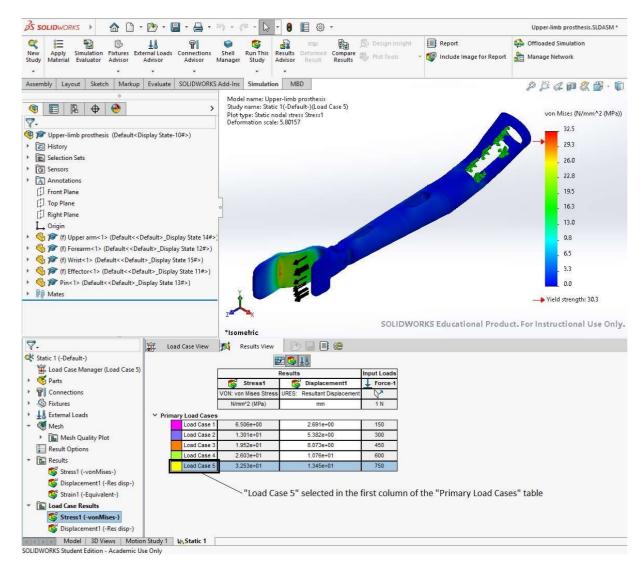


Figure 39: Color map showing the distribution of the von Mises equivalent stress at the level of the entire assembly (fifth load case: traction force of 750 N)











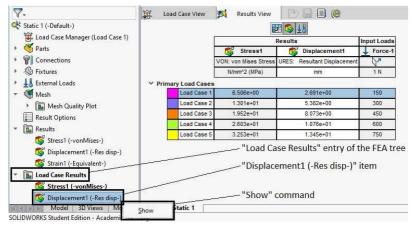


Figure 40: Selecting the distribution of the deflection to be examined

The maximum value of the von Mises equivalent stress $\sigma_{\rm eq,max}$, the maximum deflection $d_{\rm max}$, and the traction force F corresponding to different load cases are listed in the second, third and fourth column of the "Primary Load Cases" table placed at the bottom of the "Results View" tab (Fig. 43). Table 2 (see below) presents this data in a more readable format.

The plots in Figures 44 and 45 show the dependencies $\sigma_{\rm eq,max}$ vs F and $d_{\rm max}$ vs F, respectively. Both diagrams allow noticing that the mechanical response of the prosthesis is linear. In fact, the dependencies $\sigma_{\rm eq,max}$ vs F and $d_{\rm max}$ vs F are well approximated by the regressions

$$\sigma_{\rm eq,max} = 4.337 \cdot 10^{-2} \cdot F,$$
 (1)

and

$$d_{\text{max}} = 1.794 \cdot 10^{-2} \cdot F, \tag{2}$$

respectively (see the black lines in Figures 44 and 45).

It can be easily seen in Table 2 and Figure 44 that $\sigma_{eq,max}$ equals the yield strength of the PETG material Y = 30.3 MPa (as defined in the *EMERALD CAE Materials.sldmat* library – see Table 1 and Figure 18) for a traction force 600 N < F_{cr} < 750 N. This critical load results from Eq (1) as soon as the replacement $\sigma_{eq,max} = Y = 30.3$ MPa is made:

$$F_{cr} = Y \cdot 100 / 4.337 = 30.3 \cdot 100 / 4.337 = 698.64 \text{ N}.$$
 (3)











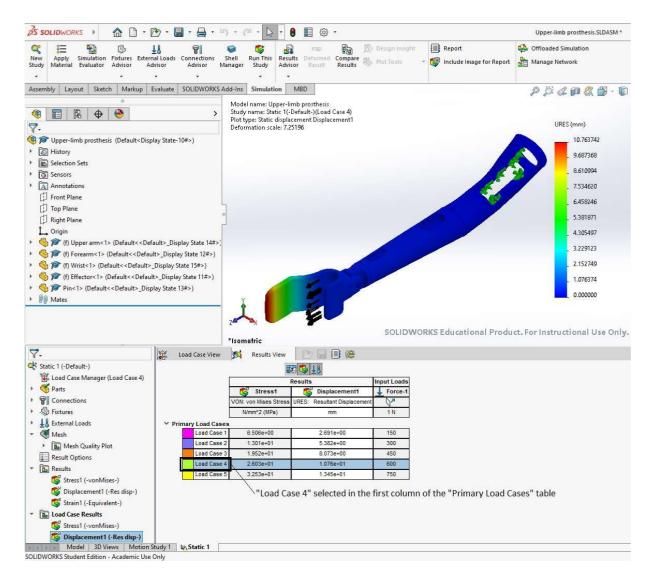


Figure 41: Color map showing the distribution of the deflection at the level of the entire assembly (fourth load case: traction force of 600 N)











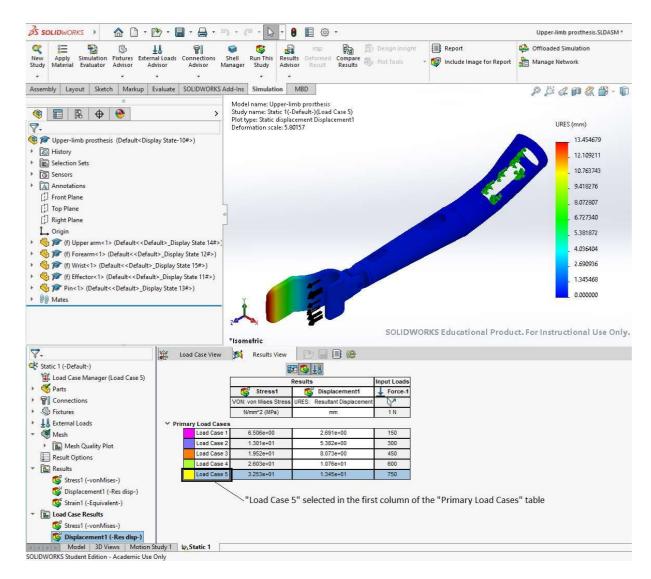


Figure 42: Color map showing the distribution of the deflection at the level of the entire assembly (fifth load case: traction force of 750 N)











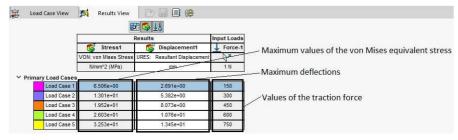


Figure 43: Maximum value of the von Mises equivalent stress, maximum deflection, and traction force corresponding to different load cases listed in the "Primary Load Cases" table

Table 2: Traction force, maximum value of the von Mises equivalent stress, and maximum deflection corresponding to different load cases (see also Figure 43)

| Load case | Traction force | Maximum value of the von Mises Maximum def | |
|-----------|----------------|---|-----------------------|
| Load Case | <i>F</i> [N] | equivalent stress $\sigma_{\sf eq,max}$ [MPa] | d _{max} [mm] |
| 1 | 150 | 6.51 | 2.691 |
| 2 | 300 | 13.01 | 5.382 |
| 3 | 450 | 19.52 | 8.073 |
| 4 | 600 | 26.03 | 10.764 |
| 5 | 750 | 32.53 | 13.455 |

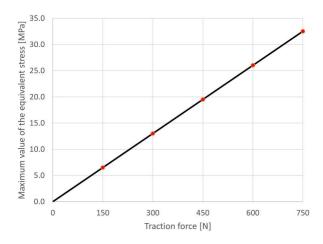


Figure 44: Dependence $\sigma_{eq,max}$ vs F: red dots – numerical results taken from Table 2; black line – linear regression defined by Eq (1)











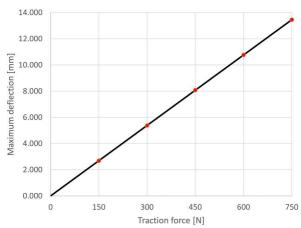


Figure 45: Dependence d_{max} vs F: red dots – numerical results taken from Table 2; black line – linear regression defined by Eq (2)

4. Suggestions for individual work

a) Evaluate the strength characteristics of the upper-limb prosthesis by simulating the distal tensile test under the hypothesis that all the components are made of PLA exhibiting an isotropic linear elastic behavior. Table 3 lists the physical and mechanical properties of this material that are relevant for the finite element model.

Table 3: Physical and mechanical properties of PLA [Far2016]

| Mass density | Elastic modulus | Poisson's ratio | Yield strength | |
|-----------------------------|-----------------|-----------------|----------------|--|
| ρ [kg/m ³] | <i>E</i> [MPa] | ν [-] | Y [MPa] | |
| 1252 | 3500 | 0.36 | 59 | |

Note: The properties listed in Table 3 are stored in the custom library *EMERALD CAE Materials.sldmat.*

b) Develop another design of the upper-limb prosthesis and evaluate its strength characteristics by simulating the distal tensile test.











References

[Far2016] Farah, S.; Anderson, D.G.; Langer, R. Physical and mechanical properties of PLA, and their functions in widespread applications — A comprehensive review. Advanced Drug Delivery Reviews 2016, 107, 367-392. [https://doi.org/10.1016/j.addr.2016.06.012]

[Kan2020] Kannan, S.; Ramamoorthy, M.; Sudhagar, E.; Gunji, B. Mechanical characterization and vibrational analysis of 3D printed PETG and PETG reinforced with short carbon fiber. In Proceedings of the International Conference on Physics and Chemistry of Materials in Novel Engineering Applications PCMNEA2020 (AIP Conference Proceedings 2270), Coimbatore, India, 6-7 February 2020; 030004. [https://doi.org/10.1063/5.0019362]

[WWW2022a] https://www.solidworks.com/

[WWW2022b] https://www.solidworks.com/product/solidworks-simulation

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The Education, Scholarships, Apprenticeships and Youth Entrepreneurship

EUROPEAN NETWORK FOR 3D PRINTING OF BIOMIMETIC

MECHATRONIC SYSTEMS

E-toolkit – 3D Printing

| Project Title | European network for 3D printing of biomimetic mechatronic systems 21-COP-0019 |
|------------------|--|
| Output | IO2 - EMERALD e-toolkit manual for digital learning in producing biomimetic manufacturing method |
| Module | 3D Printing |
| Date of Delivery | January 2023 |
| Authors | Diana BĂILĂ |
| Version | FINAL VARIANT, *24.01.2023* |











Contents

| 1 | Pro | Product 1: Personalized Orthosis | | |
|---|-----|---|-----|--|
| | 1.1 | CAD Modeling | 3. | |
| | 1.2 | STL file | 5. | |
| | 1.3 | 3D Printing software's | 6. | |
| 2 | Pro | oduct 2: Robotic Arm | | |
| | 2.1 | CAD Modeling | 16. | |
| | 2.2 | STL file | 18. | |
| | 2.3 | 3D Printing software's | 19. | |
| 3 | Pro | educt 3: 3D Fresh Printing of organ phantom for surgical applications | | |
| | 3.1 | CAD Modeling | 27 | |
| | 3.2 | STL file | 28 | |
| | 3.3 | 3D Printing software's | 29 | |
| 4 | Cor | nclusions | 38 | |
| | | | | |

This project has been funded with support from the Iceland Liechtenstein Norway Grants. This publication [communication] reflects the views only of the authors, and the Commission cannot be held responsible for any use which may be made of the information contained therein.



5









1 3D Printing toolkit for medical applications

Product 1: Personalized Orthosis – SLDPRT. file Poznan University of Technology Partner

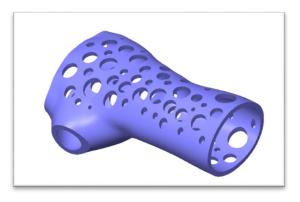


Fig.1. Personalised orthosis

1.1. CAD Modeling

CAD modeling is used by many designers to create elaborate computerized models of objects before they are physically produced. CAD stands for computer-aided design. Engineers, architects, and even artists utilize computers to assist in their design projects. Computers allow them to visualize their designs and confront problems before they have expended any of the resources necessary to put them into physical form. [1-88]

CAD modeling takes many different forms depending on the type of project. Some models are simple two-dimensional representations of various views of an object. Others are elaborate three-dimensional cross-sections that show every detail in great depth. Some CAD models are even animated, showing how all of the components of the model work together to complete its function.

Many different professions make use of computer-aided design. It is an important industrial art involved in automotive, aerospace, prosthetic, and artistic designs. The use of CAD modeling is massively widespread; anything from chairs to rockets can be designed with the aid of computer programs. Among other titles, CAD modelers are referred to as CAD monkeys,

designers, and digital information engineers. A single CAD file, and continually tweaked until the object is ready for production.

can b

can be made, edited











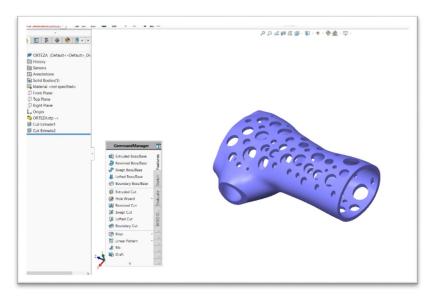


Fig.2. SolidWorks - SLDPRT. file

SolidWorks is a solid modeling computer-aided design (CAD) and computer-aided engineering (CAE) application published by Dassault Systèmes, as in figure 2. [1]

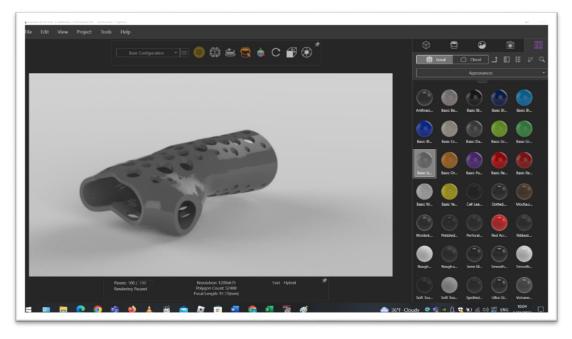


Fig.3. SolidWorks Visualize 2019 – orthosis with different texture mapping











The CAD software permits to realize the three-dimensional models using different geometric entities such as, lines, rectangle, curves surfaces interconnected to a multitude of points in 3D space.

The 3D models can be realized by algorithms, using CAD software or by Reverse Engineering using a 3D scanner that collects information's concerning the dimensions and the 3D shape of the object. SolidWorks Visualize 2019 permits their surfaces to be further defined with texture mapping, as in figure 3 [1].

1.2. STL file

To design the personalised orthosis, it was starting a new work session in SolidWorks, on click "Part", because it's a single design component. After design the personalised orthosis, it will be saved with name "Personalised Orthosis", in SLDPRT format. For manufacture using 3D Printing technology, the solid part is converted in STL file, and it will be saved such as .stl and must to choose from properties menu the resolution (coarse, fine or custom) and it was choose fine quality for meshing the product, such in Figure 4. Total triangles are 52426 used for meshing.[1-88]

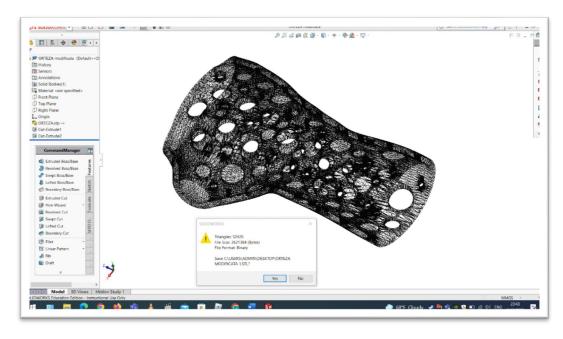


Fig.4.Orthosis meshing - STL. file











1.3. 3D Printing software's

Additive Prototyping Technologies (AM) differ fundamentally from material removal processing technologies (cutting, EDM, laser processing) and redistribution processing technologies material (casting, injection, forging, stamping) by the fact that the parts are obtained by adding layer by layer material using a CAD file.

These technologies have emerged grace a result of the achievements and advances made in the field of fine mechanics, numerical control, laser technology, computers, software, and the new materials development.

The specificity of these additive manufacturing processes is their ability to make parts and complex three-dimensional objects, starting from a CAD file, without the need for it use of machine tools or certain tools. The basic element of prototype additive manufacturing technologies is "the section". [1-86]

The pieces are quantified in sections and made using a repetitive process of construction, section by section, reducing a three-dimensional problem to one flat. This dimensional reduction leads to a decrease in accuracy and quality surfaces due to the scale effect.

The steps required for the additive manufacturing of a part are as follows:

- -designing the three-dimensional (3D) model of the part, using a design program computer aided (CAD);
- -transferring the CAD model to the sectioning processor. The best-known method of sectioning is the approximation of the model with flat triangular elements.
- sectioning the 3D virtual model with parallel planes to the working plane of the rapid manufacturing machine of prototypes and generation of orders for control equipment of the machine.
- -the construction of the part (material, supports required during the model, how will be added a new layer, marking the contours for each section, marking the area between the exterior and interior contour of a section.
- cleaning and finishing of the part (operations in which the supports used at construction and excess material are eliminated).[1-88]

Regarding solid CAD modelling, Additive Manufacturing systems are becoming an important and motivating factor for companies that produce solid modelling systems, such as: Solidworks, Unigraphics, I-DEAS, Catia, Inventor, Onshape, AutoCAD, Pro / Engineer, etc











The best software used by FDM (Fused Deposition Modeling) printers are Ultimaker Cura, BCN 3D Cura, Voxelizer, Z-Suite, etc and for SLA (Stereolithography)/DLP (Digital Light Processing) printers are FormLabs, Photocentric, etc.

Using https://ultimaker.com/en/resources/manuals/software and downloaded free software https://ultimaker.com/en/products/ultimaker-cura-software, than it must to obtain the g-code file necessary to print the part. The first step consist in open Ultimaker Cura software and to introduce by drag the part, as stl.file, such in the Figure 5. The software permits to choose the 3D Printer that it is necessary to print, and in this case, it is used Ultimaker S5. For printing, it must to use a cable or a card memory or via wireless to connect the 3D printer to laptop to put in function the 3D Printer.[1-88]

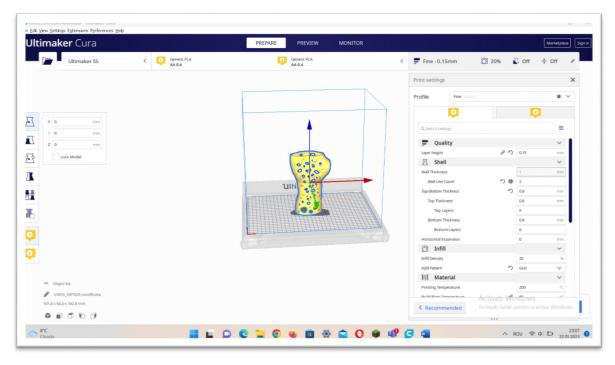


Fig.5. Open Ultimaker Cura software and introduce the STL. file of part

The software permit the move of the part on the work platform after the X,Y,Z axis, the change of the part scale after X,Y,Z axis, such as Figure 6. The rotation of the part after the X, Y, Z axis, the multiplication of the parts on the work platform and the mirror parts printing, it is permitted by the software.











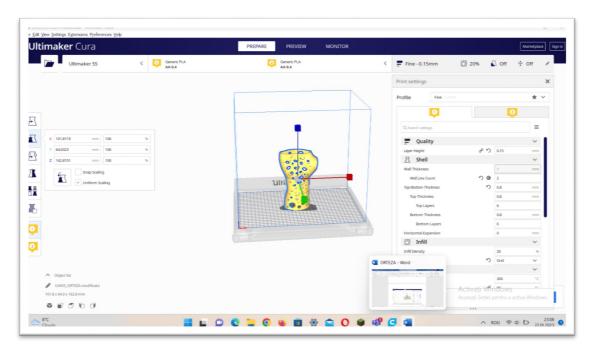


Fig.6. Change the part scale, after X, Y, Z axis

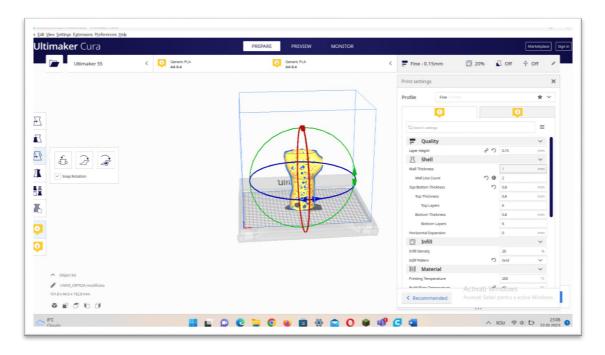


Fig.7. Rotation of the part after X, Y, Z axis











The software permit to choose for printing different materials, as PLA, ABS, PET, etc. For the personalised orthosis, it was choosing ABS materials with the mechanical properties given in the Table 1.[1-88]

ABS and PLA are the most common FDM (Fused Deposition Modeling) printed materials and are typically similar in cost. ABS has superior mechanical properties but is harder to print compared to PLA. Material properties can be chosen using the free site https://www.totalmateria.com/page.aspx?ID=Home&LN=RO

Table 1. The mechanical properties of Acrylonitrile Butadiene Styrene (ABS)

| Properties | Values | Units |
|---------------------------------------|-----------|---------|
| Density | 1.0-1.4 | g/cm3 |
| Poisson's Ratio | 0.35 | - |
| Shear Modulus G | 1,03-1,07 | GPa |
| Melting Temperature | 200 | °C |
| Glass transition temperature | 105 | °C |
| Thermal Conductivity | 0,25 | W/m-K |
| Extruded Temperature | 200-230 | °C |
| Heat Deflection Temperature, 1,81 MPa | 81 | °C |
| Young's modulus | 1,79-3,2 | GPa |
| Tensile Strength | 29,8-43 | MPa |
| Compressive Strength | 76-78 | MPa |
| Elongation at Break | 10-50 | % |
| Flexural modulus | 2,1-7,6 | GPa |
| Hardness Shore D | 100 | |
| Izod Impact Strength | 58 | kJ/m2 |
| Yield Strength | 28-120 | MPa |
| Standard Tolerance | +/-0.05 | mm |
| Biodegradable | - | - |
| Melt flow | 12-23 | g/10min |
| Rockwell Hardness | R102-R104 | |

Due to its lower printing temperature is easier to print with and therefore better suited for parts with fine details. ABS is best suited for applications where strength, ductility, machinability and thermal stability are required. ABS is more prone to warping. The mechanical properties of ABS are presented in Table 1.











For 3D Printing process was used only an extruder, the extruder 1 (Fig.8), but in generally we can work with 2 extruders, one for supports and other for part manufacture, as in the Fig. 9. The software permit to custom the 3D Printing process of parts, as in Figure 10 (a and b) or to use the recommended parameters for part manufacturing as in Figure 11.[1-88]

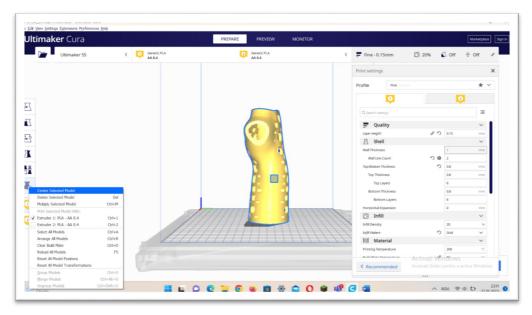


Fig 8. 3D Printing Extruder chosen

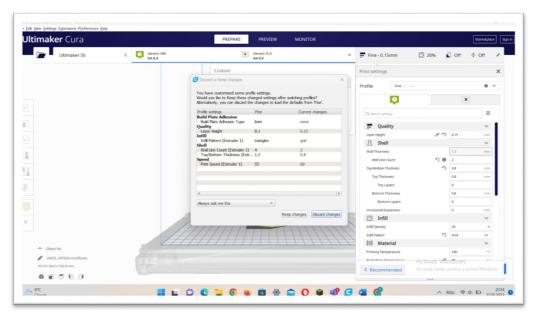












Fig.9. Choosing the ABS filament for 3D Printing

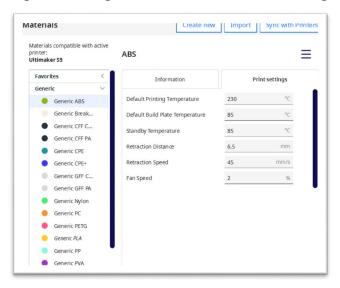


Fig. 10a. Printing setting for ABS material







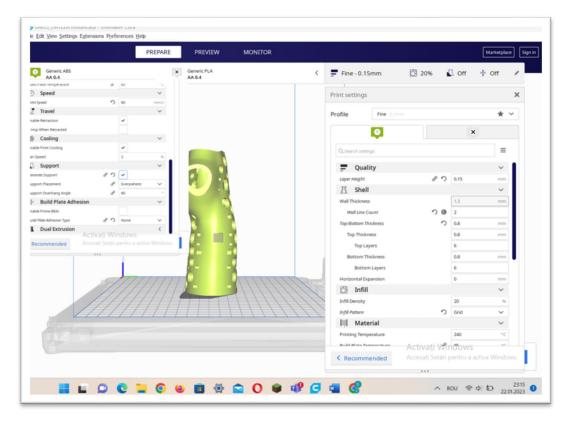


Fig. 10b. Manufacturing parameters for custom 3D Printing without supports









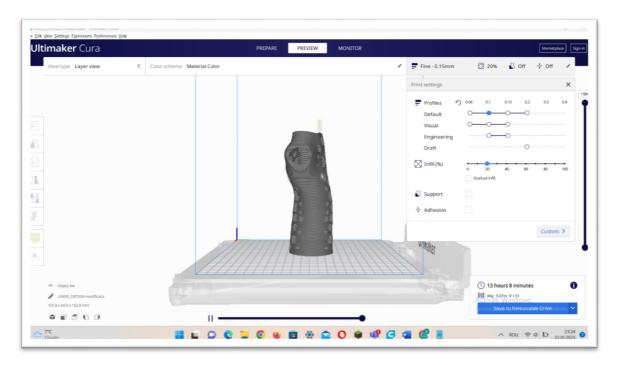


Fig.11. Recommended manufacturing parameters for the part by the software

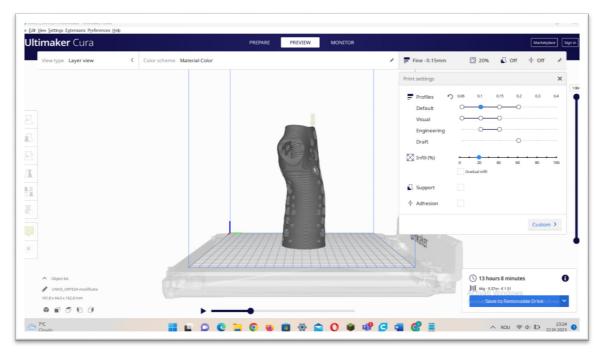


Fig.12. Preview the manufacturing 3D Printing process











It must click the blue button slice to slicing the parts. The software gives information's concerning the time necessary for manufacturing (13 hours and 8 minutes), the cost of the part (1.51 euros if 1kg ABS filament cost of 25 euros) and the material consumption (66 g, filament length used 9.37 m). The software permit to used supports if it necessary to obtain parts with great accuracy or without supports if it must obtain part in a shorter time. The software permit to preview by a small video, the simulation concerning the 3D Printing process, as in the Figure 12.[1-88]

For saving the part file, the software Ultimaker Cura it necessary to click on Save Project, as in Figure 13, then it will obtain the Summary- Cura Project, as in the Figure 14, and it will save as

3mf. file Orthosis, as in the Figure 15.

The software permit export file (Figure 16) with different extensions, and it was choose the

extension file - g-code orthosis necessary to 3D Printing, as in Figure 17. In figure 18, it is presented how look the g-code for orthosis part. For time of printing is 13 hours and 8 minutes and the filament consumable is 66 g, length 9.37m, and the cost of part is 1.51 euro, if considered that the filament cost is 25 euro/kg.











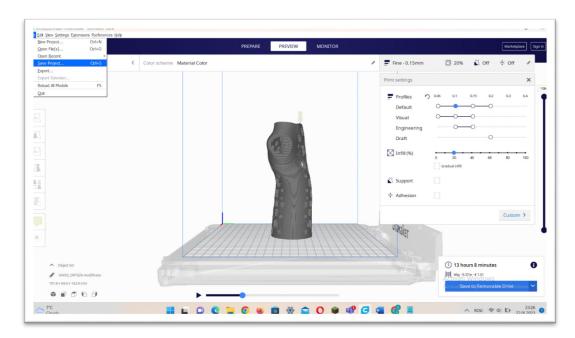


Fig.13. Save Project

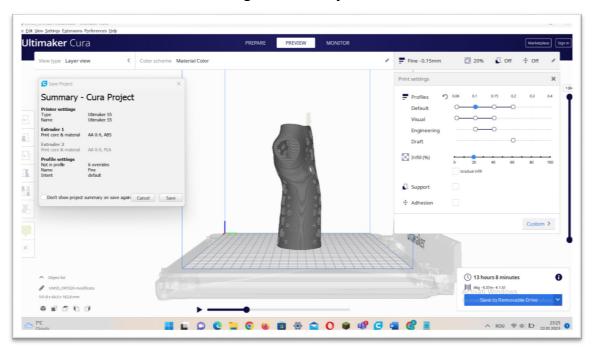


Fig.14. Summary- Cura Project











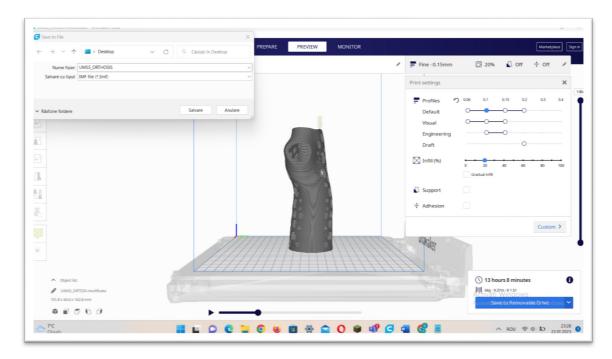


Fig.15. Save project as 3mf. file

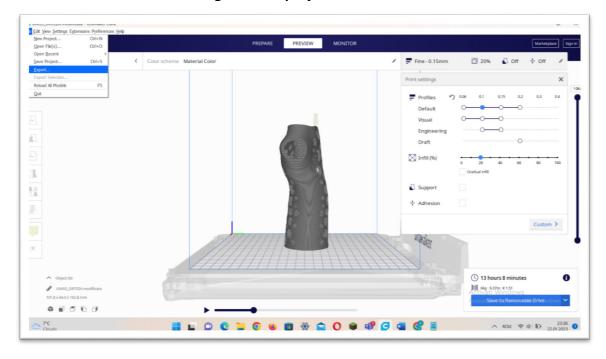


Fig.16. Export file











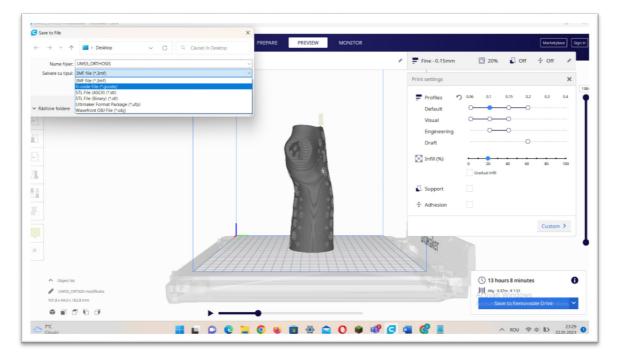


Fig.17. Different extension for file export

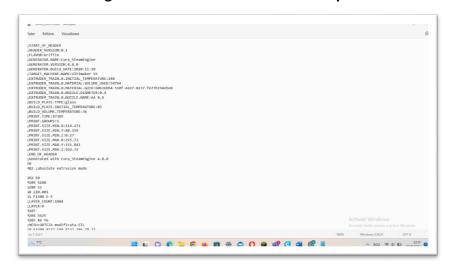


Fig.18. G-code file for personalized orthosis part













Fig.19. Personalized Orthosis printed by FDM technology

Product 2: Robotic Arm – ASM, SLDASM. file Poznan University of Technology Partner

2.1. CAD Modeling

Many CAD files (13 elements) must be made, designed and saved as SLDPRT files and then will

be assembled using Assembly to obtain the robotic arm, save as ASM, SLDASM file, as in the Fig.20. is ready for production.[1-88]









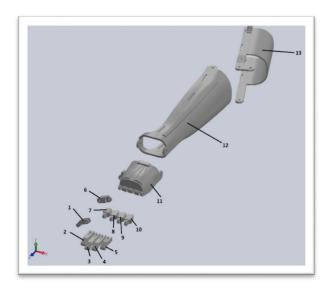


Fig.20. Exploded View - Robotic Arm

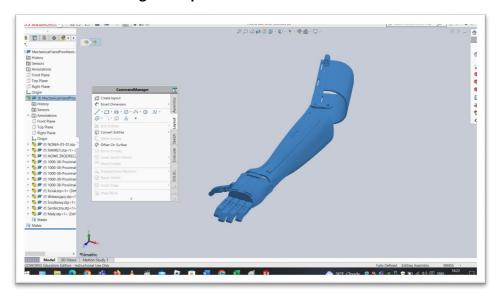


Fig.21. Robotic arm assembly - ASM, SLDASM. File

In the figure 21 is presented robotic arm assembly (all 13 elements), saved as ASM, SLDASM file. file to establish if the parts were well designed. In figure 22, it was used SolidWorks Visualize 2019, that permit to choose different texture mapping (in function of the material used, plastic, metallic, glass, etc.) for the robotic arm.[1-88]











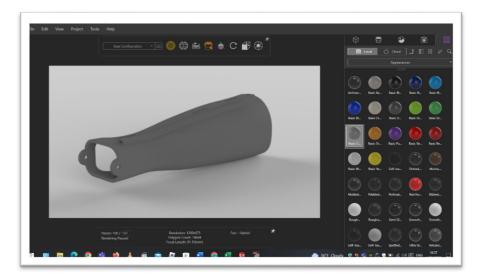


Fig.22. SolidWorks Visualize 2019 – robotic arm with different texture mapping

2.2. STL file

For manufacture using 3D Printing technology, the solid part is converted in STL file, and it will be saved such as .STL file and must choose from properties menu the resolution (coarse, fine or custom) and it was choose fine quality for meshing the product, such in Figure 23. Total triangles are 109616 used for meshing.[1-88]

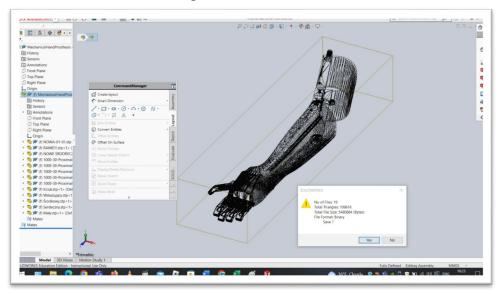












Fig.23.Robotic Arm - STL. file

2.3. 3D Printing software's

The material chosen to be used for this product is PLA filament, having the mechanical properties presented in table 2. PLA is ideal for 3D prints where aesthetics is important.

Table 2. The mechanical properties of PLA (Polylactic Acid)

| Properties | Values | Units |
|------------------------------|---------|-------|
| Density | 1.25 | g/cm3 |
| Poisson's Ratio | 0.36 | - |
| Shear Modulus G | 2.4 | GPa |
| Melting Temperature | 173 | °C |
| Glass transition temperature | 60 | °C |
| Thermal Conductivity | 0.13 | W/m-K |
| Extruded Temperature | 160-220 | °C |
| Heat Resistance | 110 | °C |
| Young's modulus | 3.5 | GPa |
| Tensile Strength | 61.5 | MPa |
| Compressive Strength | 93.8 | MPa |
| Elongation at Break | 6 | % |
| Flexural strength | 88.8 | MPa |
| Hardness Shore D | 85 | Α |
| Impact Strength | 30.8 | kJ/m2 |
| Yield Strength | 60 | MPa |
| Standard Tolerance | +/-0.05 | mm |
| Biodegradable | yes | - |











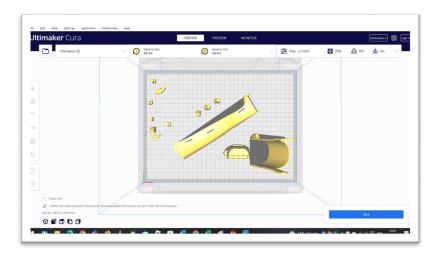


Fig.24. Drag the STL. files on the worktable of the 3D Printer using Ultimaker Cura

In the Figure 25 is shown the PLA filament choosing for 3D Printing and in the figure 26 are presented the printing setting for PLA filament used for FDM process.[1-88]

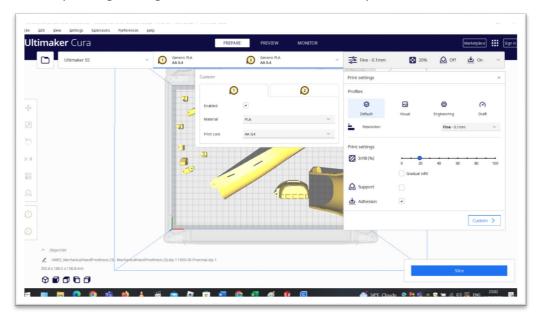


Fig.25. PLA filament choosing for 3D Printing









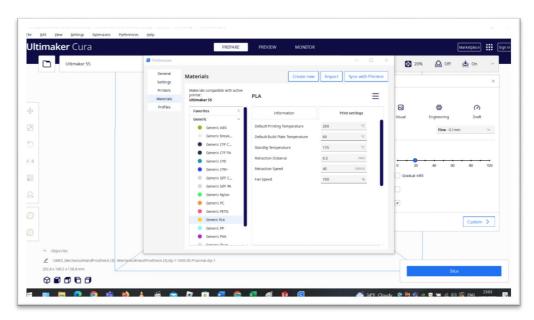


Fig.26. Printing setting for PLA material

In figure 24, all components of robotic arm saved as STL. files are drag on the worktable of the software, because are great dimensions and the Ultimaker S5 table does not permit, we can print simultaneous files at the scale 60%, as in the Figure 27 or we can print in multiples stages at the scale 100%. For 3D Printing, were used two extruders and was used the recommended manufacturing parameters given by software and were selected the supports. It must click the blue button slice to slicing the parts.[1-88]







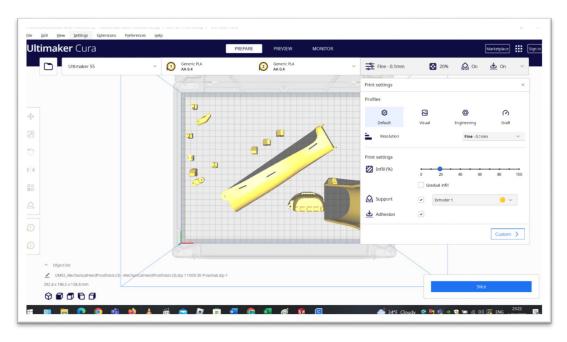


Fig.27. Prepare 3D Printing using two extruders and click slice

For the manufacturing of part exist two modes: recommended by software or custom, where it can personalise the 3D Printing process in function of the materials, the supports necessary, the speed, the temperature, the infill density of the support material. In figure 28, it is presented the recommended manufacturing parameters for robotic arm given by Cura software. In figure 29 is presented the preview of the manufacturing process, it is a small simulation.

The part can be saved as project 3mf. file repair as in Fig.30 and the summary report is shown in Fig.31. The file can be exported using different extensions: stl (ASCII and BINARY), g-code, obj, 3mf and ufp, such in figure 32. In figure 33 is presented the g-code file for Robotic Arm

and in figure 34 is the printed robotic arm at scale 1:1. After the printing of the part, the supports are eliminated, and the surfaces are cleaned. The surfaces can be manufactured by different classical mechanical processes, such as drilling, milling, etc. The time for the printing process is 1 day 18 hours 39 minutes, the filament consumable is 157 g, filament length used is 19.82 m, the filament cost is 3.14 euros, if considered the PLA filament cost 25 euro/kg.











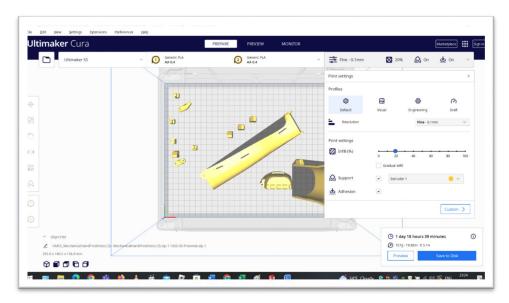


Fig.28. Recommended manufacturing parameters for the part by the software

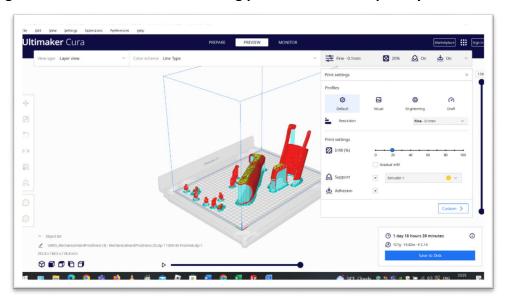


Fig.29. Preview the manufacturing 3D Printing process









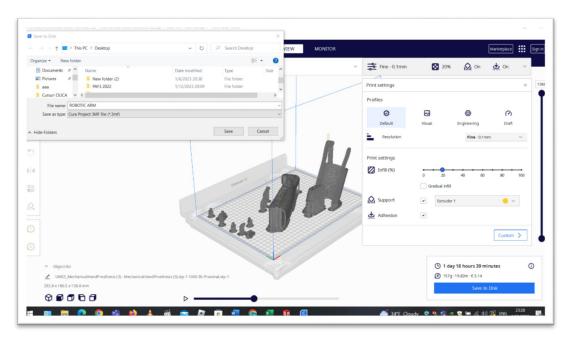


Fig.30. Save project as *3mf. file

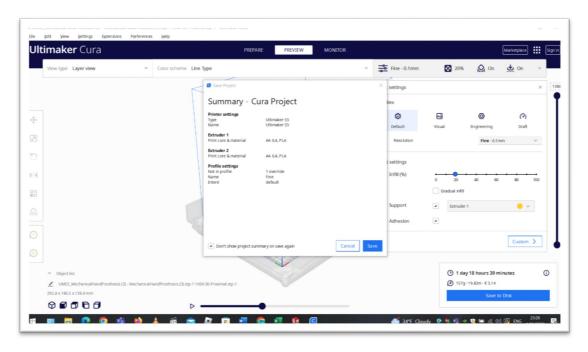


Fig.31. Summary- Cura Project











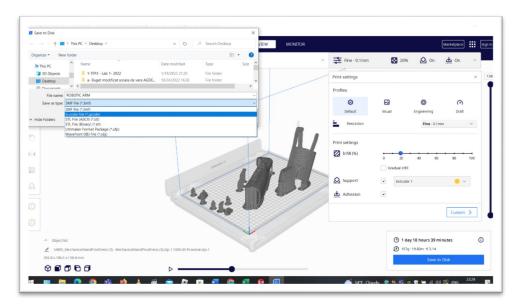


Fig.32. Different extensions for file export



Fig.33. G-code file for Robotic Arm



Fig.34. Robotic Arm printed by FDM technology and assembled











Product 3: 3D Fresh Printing of organ phantom for surgical applications — site https://www.embodi3d.com/

Physical organ models are the objects that replicate the patient-specific anatomy and have played important roles in modern medical diagnosis and disease treatment. 3D printing, as a powerful multi-function manufacturing technology, breaks the limitations of traditional methods and provides a great potential for manufacturing organ models.

Fresh 3D Printing (Freeform Reversible Embedding of Suspended Hydrogels) is an additive manufacturing technique for manufacturing different organ phantoms which can mimic the corresponding soft living tissue. [1-88]

The technology 3D Fresh Printing is similarly with the technologies SLA and DLP, only that used silicones or hydrogels, that permit to print different human organ models with the real consistency of the respective organs, that permit to help the students to University of Medicine to study their properties and to prepare the surgical operation stages planning, implantable epidermal devices, patient-specific pulse oximeters and in the tissue engineering applications. The printer must be modified, such as Tobeca 333, (Tobeca, France), that used the software Simplify 3D and as material a mono-component silicone by Elkem Silicones, France (AMSil 20101).

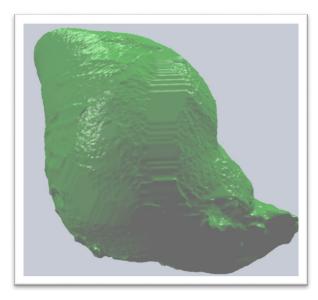


Fig.35. Liver model for printing











The nature of FRESH printing offers the capability to 3D print object using layer-bylayer, non-planar or freeform approaches. The latter one produces geometries that are not possible to achieve in traditional 3D printing. Additionally, it solves one of the most tedious processes of 3D printing, which is to guarantee that the platform is completely flat, since the object can be manufactured in any location of the support bath. In general, the materials used is the thermoreversible Pluronic F-127 based support bath supplied by Sigma Aldrich, USA. Fresh 3D printing is a particular type of DIW embedded 3D printing EMB3D technique. [1-88]

For the surgical operation stages planning, we can use the technology SLA and DLP, that are most simple to used and can permit the 3D Printing with a great accuracy the complex parts. In the SLA (Stereolithography) and DLP (Digital Light Processing) technologies are used photocurable vinyl- or epoxy- functional oligomers for photopolymerization. In table 3 are presented the mechanical properties of Bisphenol A Ethoxylate Diacrylate resin. Other resins used in SLA manufacturing are the polyurethane resins.

Table 3. The mechanical properties of Bisphenol A Ethoxylate Diacrylate

Bisphenol A Ethoxylate Diacrylate

INTRODUCTION

EBECRYL 150 is an ethoxylated bisphenol A diacrylate commonly used as reactive diluent in UV/EB cure applications. EBECRYL 150 can improve the cure response, hardness, and chemical resistance of UV/EB curable coatings and inks while maintaining good adhesion, and without imparting brittleness.

PERFORMANCE HIGHLIGHTS

EBECRYL 150 is characterized by:

- High reactivity
- Moderate viscosity
- High refractive index

UV/EB curable formulated products containing EBECRYL 150 are characterized

- Hardnes
- Chemical resistance
- Good adhesion

The actual properties of UV/EB cured products also depend on the selection of other formulation components such as oligomers, additives and photoinitiators

| SPECIFICATIONS(1) | VALUE |
|---|---------------|
| Acid value, mg KOH/g, max. | 5 |
| Appearance | Clear liquid |
| Color, Gardner scale, max. | 2 |
| Viscosity, 25°C, cP/mPa·s | 1150-1650 |
| TYPICAL PHYSICAL PROPERTIES | |
| Density, g/ml at 25°C | 1.14 |
| Flash point, Setaflash, °C | >100 |
| Functionality, theoretical | 2 |
| Refractive index (n _D at 20°C) | 1.5294 |
| Vapor pressure, mm Hg at 20°C | <0.01 |
| TYPICAL CURED PROPERTIES(2) | |
| Tensile strength, psi (MPa) | 6300 (43) |
| Elongation at break, % | 9 |
| Young's modulus, psi (MPa) | 180000 (1241) |
| Glass transition temperature, °C(3) | |











3.1. CAD Modeling

For 3D Printing of physical organ models, the medical images are first acquired through computer tomograph CT, magnetic resonance imaging MRI. Through the above procedures, the original image data, usually in DICOM (Digital Imaging and Communications in Medicine) format, will be obtained and then can be processed.

Image processing is a process of transforming DICOM images into 3D digital models. It is also a broad concept, including image segmentation, computer aided design (CAD) and format conversion.

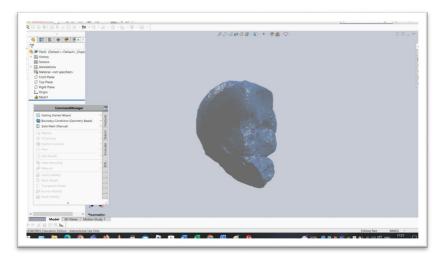


Fig.36. STL. file – liver phantom

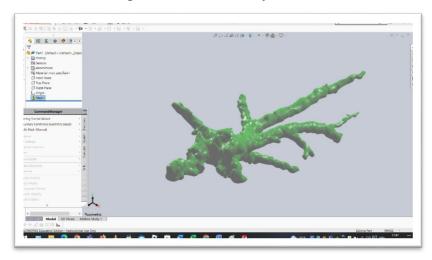


Fig.37. STL. file - blood vessel











3.2. STL file

The file formats that 3D printers can accept are limited to several special 3D dataset files, mainly the Standard Tessellation Language (STL) format and some newer formats called Additive Manufacturing File Format (AMF) or 3D Manufacturing Format (3MF). The model data must be converted into files in these formats before it can be 3D printed.

There are several software can meet the demands of image processing, ranging from interactive medical image processing software like Mimics (Materialise), D2P (3D Systems), and CAD model processing software like Magics (Materialise), Geomagic Studio (3D Systems) and SolidWorks (Dassault Systems). In many cases, using multiple software together can integrate different functions.

For 3D Printing of the liver are 6 components, they are 6 different STL. Files (liver and blood vessels), that must be assembled and saved as ASM, SLDASM. file and printed 3D. We obtain the STL. files, such in the figures 36 and 37.

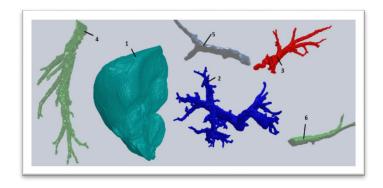


Fig.38. Exploded View – Liver phantom

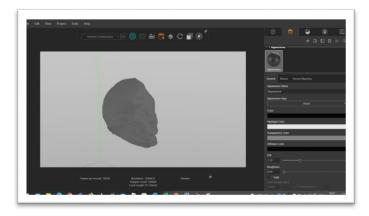


Fig. 39. SolidWorks Visualize 2019 - Liver phantom with different texture mapping











In Figure 38, it is presented the explode view of the components of liver phantom. In the Figure 39, it presented different texture mapping chosen, using SolidWorks Visualize 2019.

3.3. 3D Printing software's

For printing it used a SLA printer, FormLabs Form 2 and the free software PreForm and the resin chosen was Flexible and the layer thickness was 0.05 mm, such in Fig. 40.

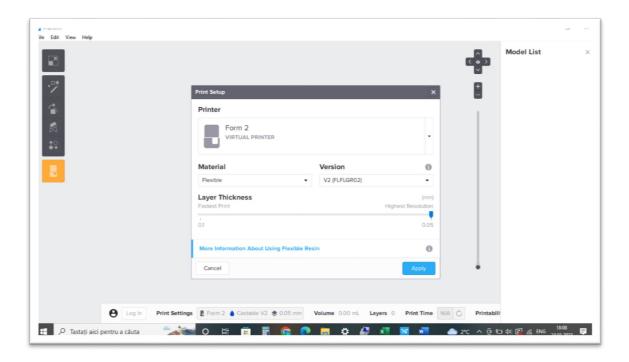


Fig. 40. Software PreForm, 3D printer, photopolymerisable resin and layer thickness chosen

In figure 41, it can click orientation to move the part on the worktable, in figure 42, it can chosen the supports necessary to sustain the part during the 3D Printing process. The layout chosen is presented in figure 43 and to print 3D it must to click on the orange button – Start a print, as in figure 44.









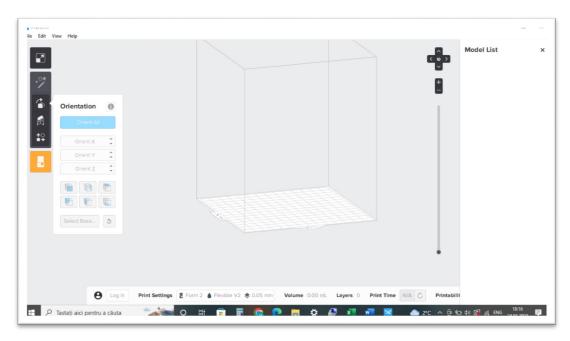


Fig.41. Orientation X,Y,Z on the worktable of the part

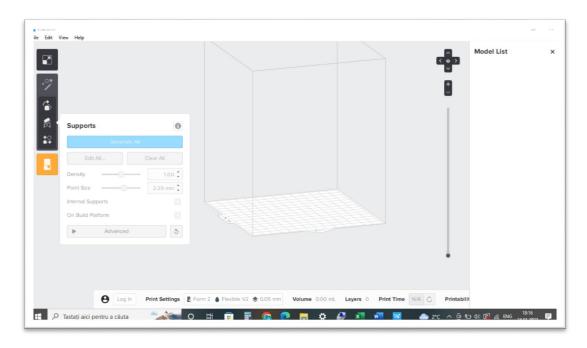


Fig.42. Supports chosen to sustain the part during the 3D Printing process











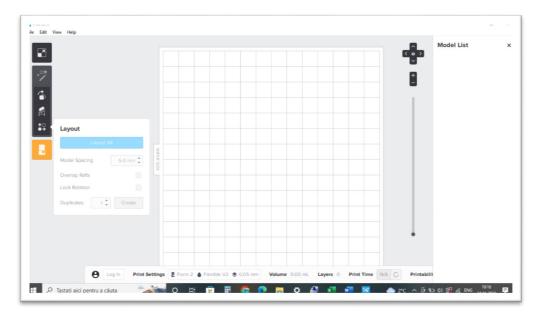


Fig.43. The layout chosen

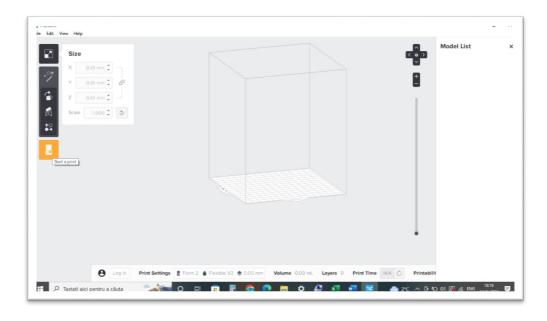


Fig.44. The orange button – Start a print











In figure 45, it was dragging the liver phantom STL. file into the worktable of the 3D Printer, but the part has very great dimensions in comparison with the worktable space, it becomes red coloured.

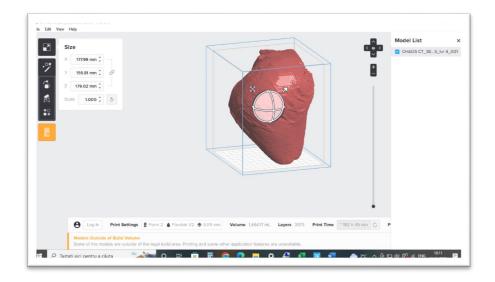


Fig.45. Drag the liver phantom STL. file on the worktable

In this case, it was changed the scale at 1:2 and was calculating orientation and generating the supports as in figure 46. [1-88]

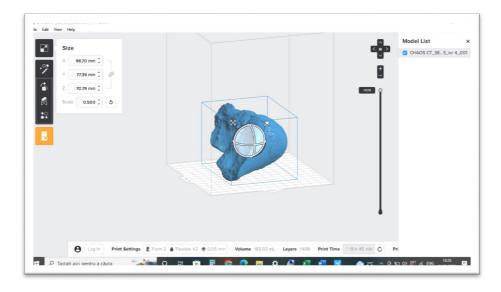


Fig.46. Change the scale at 1:2 and was calculating orientation and generating the supports











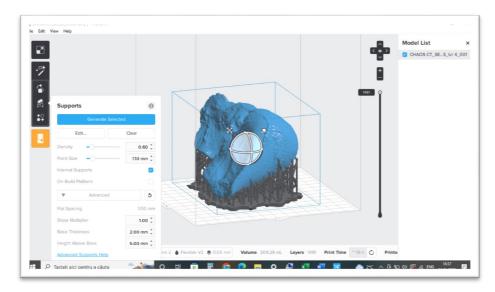


Fig.47. Calculating orientation and generating supports

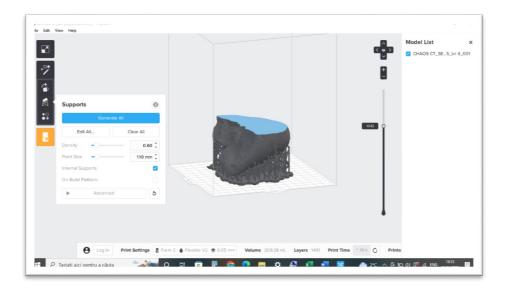


Fig.48. Surface printed at the layer 1042

For Orientation and Supports, it must click on the respective buttons and the program realized them automatically or we can realize them manually, such in figure 47. The program permit to see the slicing of the part, each layer, specify the number of the layer and the surface











coloured with blue, that is printed at the layer 1042, such in figure 48. The program shows the resin volume used 209.28 mL, nb of layers 1491 and print time approximative 19 hours.

In figure 49, the printing setting of the part liver are saved such as LIVER.FORM using the software PreForm. For 3D printing of the part, it must click on the orange button to print, such in figure 50, after connecting the printer on-line, or with a cable to the laptop.

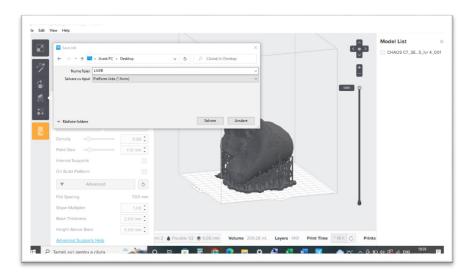


Fig.49. Save the file as Liver with the extension .FORM

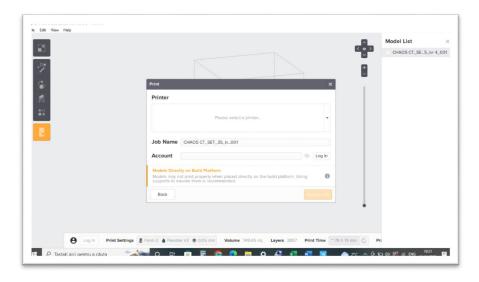


Fig. 50. Click on the orange button to print











In figure 51, it was dragging the blood vessel STL. file into the worktable of the 3D Printer and it was changed the scale at 1:2 and was calculating orientation and generating the supports as in figure 52.

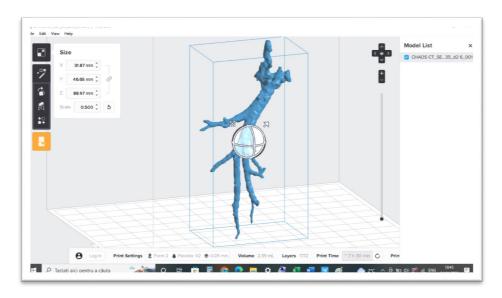


Fig.51. Drag the blood vessel STL. file on the worktable platform

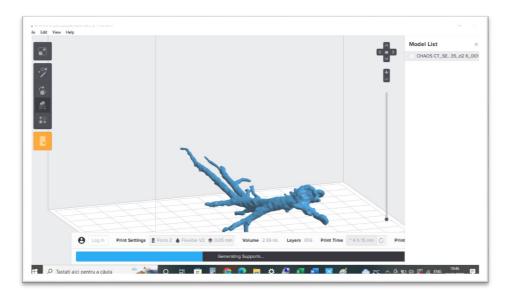


Fig.52. Calculating orientation and generating supports

First, are realized the supports, such in Figure 53 and then the part such in Figure 54.











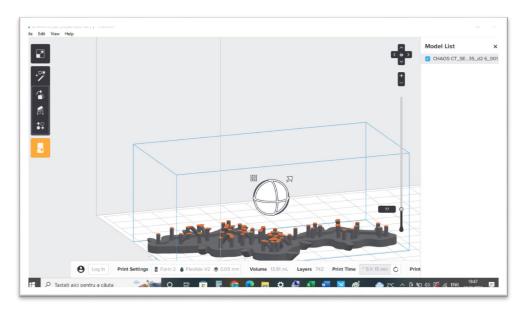


Fig.53. Supports generating

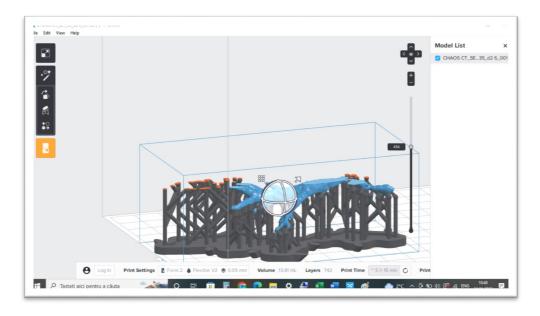


Fig.54. Part generating

In figure 55 was saved the file as Blood Vessel .FORM file and in figure 56 was click on the Print command of the part and the 3D Printer will manufacture the part. Specifically of the SLA technology is that the parts are manufactured upside down.











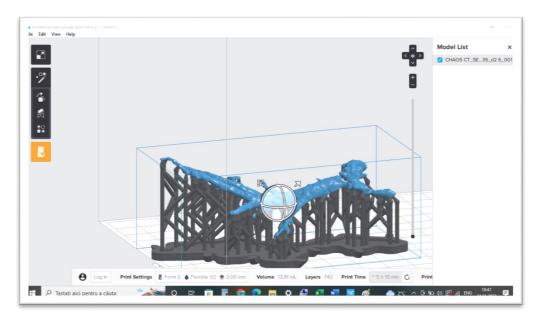


Fig.55. Save the file as Blood Vessel .FORM file

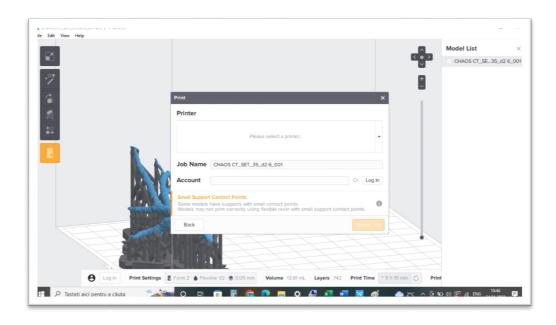


Fig. 56. Print command of the part to 3D Printer

In the figure 57 is presented the liver phantom printed 3D using the SLA technology. After printing the parts, are eliminated the supports and the parts are cleaned in isopropyl alcohol











and then are introduced in UV furnace to grow the mechanical properties during 30 minutes at the temperature of 210°C.

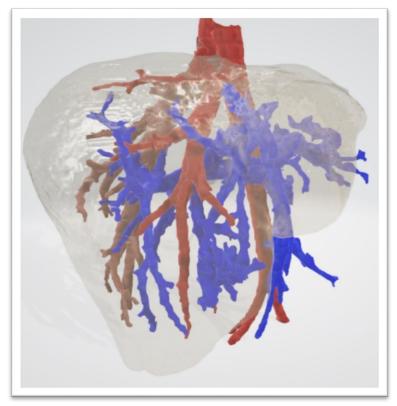


Fig.57. Liver phantom with blood vessels

4. Conclusions

In the future, further research on both multi-material and multi-colour prototypes could be performed, focusing on additive manufacturing technologies based on different silicones and plastic materials with different colours, necessary for different medical prothesis and devices. The use of different silicones would be interesting in order to manufacture more complex phantoms, in which not only the desired organ is 3D printed, but also the surrounding anatomical structures. For example, the tumour or blood vessels by changing the component ratios. [1-88]

The implications of the present research would be interesting for the manufacture of phantoms to be used in research and industry: medical imaging, preoperative surgical planning in hospitals, etc.











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MECHATRONIC SYSTEMS

E-toolkit – New materials used for the developed biomimetic mechatronic systems

| Project Title | European network for 3D printing of biomimetic mechatronic systems 21-COP-0019 |
|------------------|--|
| Output | IO2 - EMERALD e-toolkit manual for digital learning in producing biomimetic manufacturing method |
| Module | Database used for the smart (intelligent) materials properties |
| Date of Delivery | January 2023 |
| Authors | Diana BĂILĂ, PUB |
| Version | FINAL VARIANT, *27.01.2023* |











Contents

Total Materia used for determination of the materials properties

| 1. Quick search for alloys | 3. |
|---|-----|
| 2. Advanced research for alloys | 8. |
| 3. Algorithms used for identification the unknown metals | 15. |
| 4. Advanced research for polymers, ceramics and composite materials | 18. |
| 5. Conclusions | 23 |
| | |
| References | 23 |











Total Materia used for determination of the materials properties.

1 Total Materia database – Quick search for alloys

Total Materia is the world's most comprehensive materials database, having more than 20,000,000 property records for over 450,000 metallic and non-metallic materials presented in 26 languages. This database is world class quality, service and support, being trusted in over 160 countries, the smallest companies to global industry leaders all receive our complete specialist technical support. Total Materia is proprietary algorithms for the identification of unknown materials, using composition data from analytical sources, find matching materials, property data and equivalents in just seconds. This database is the largest single collection of advanced property data on the planet, having more than 150,000 materials with stress strain, fatigue data and much more for the design community, being a free page. This database permits lightning fast access for finding and comparing equivalent materials, existing international cross-references for 450,000 materials from 74 standards providing over 15,000,000 material connections.

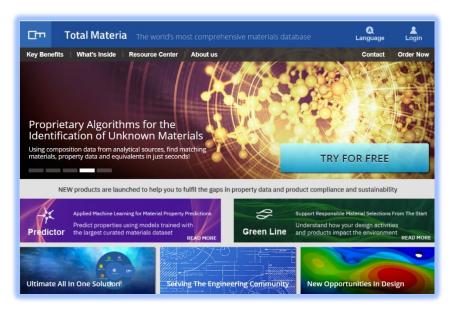


Fig.1. Total Materia database











Total Materia database help solve diverse engineering challenges from the simplest to the complex, being used in: medicine industry, aerospace industry, energy industry, automotive industry, machinery industry, engineering industry, diversified.

By example, for the alloy Ti6Al4 V, we want to know the chemical composition and the mechanical properties, and we click on Advanced Search, as in the Figure 2.

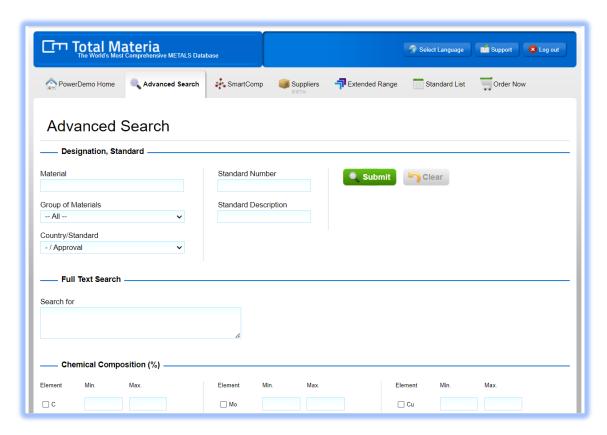


Fig.2. Advanced Search

In the figure 3, it is presented the choice of the standard in function of the country and group of materials.

It was choosing the alloy Ti6Al4V, making part of Titanium materials and was choose European Union standard, as in Figure 3. It must specify the material type, as example Bulk Materials, in Figure 4.











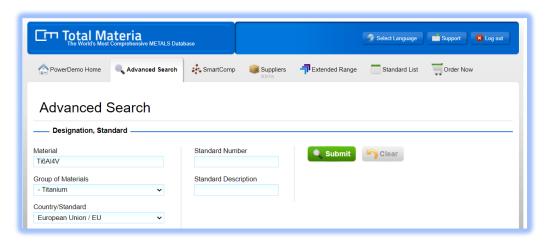


Fig.3. European Union standard choice

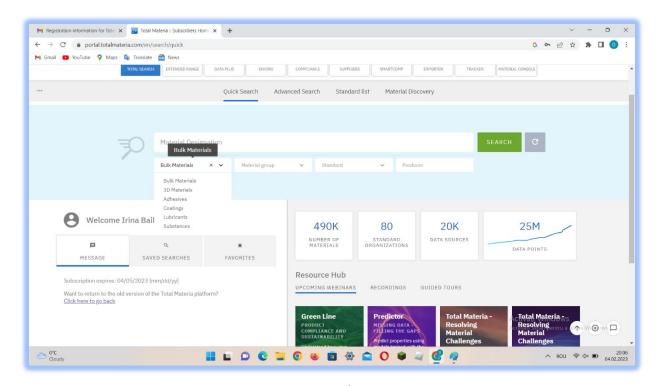


Fig.4. Material type

In figure 5, it is specifying the material group and in this case, nonferrous alloys and European standard choice, as in figure 6.











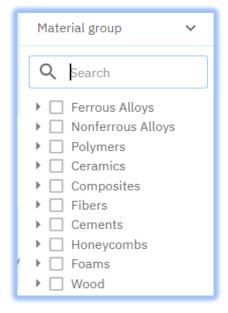


Fig.5. Material group

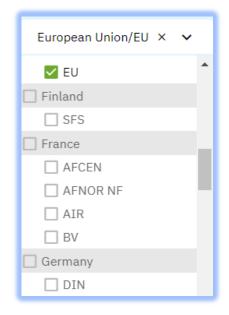


Fig.6. European standard choice

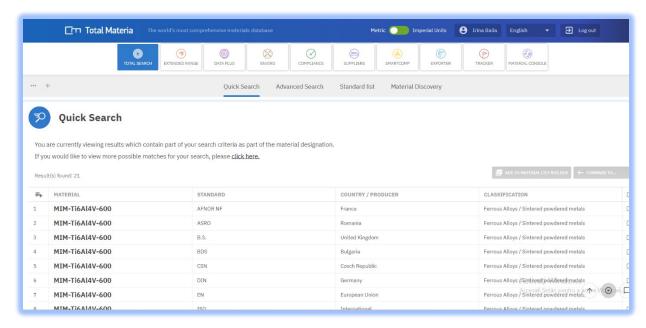


Fig.7. Different Ti6Al4V producers

When we give a quick search, as in figure 7, are presented different Ti6Al4V producers from different countries and using different standards.









Fig. 8. Ti6Al4V standard Fr AFNOR NF-Mechanical properties

The results it is the mechanical properties of the alloy Ti6Al4V, conforming of FR AFNOR NF standard, as in figure 8 and figure 9.



Fig.9. Mechanical properties Ti6Al4V at the temperature between 0-30°C

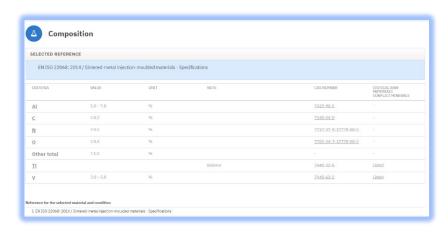


Fig. 10. Chemical composition of Ti6Al4V











In figure 9, the database gives us all information about the mechanical properties of the alloy Ti6Al4V in function of the temperature used in the process where it is used this material. In figure 10, the database shows us the chemical composition of the alloy Ti6Al4V.

2. Total Materia database – Advanced Research for alloys

In the case of Advanced Research, by example for the Ti6Al4V, producer Vday Additive Manufacturing Technology Co., it is given the classification of different Ti alloys producers, as in figure 11.

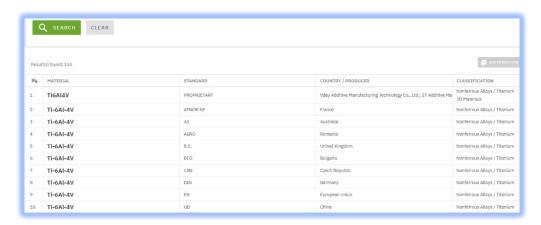


Fig.11. Ti6Al4V alloy used in Additive Manufacturing

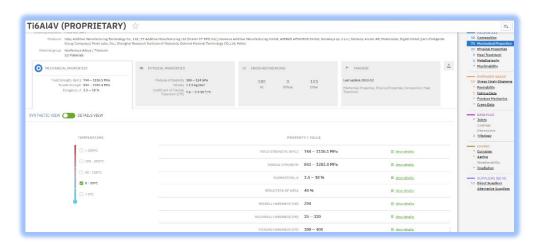


Fig.12. Mechanical properties of Ti6Al4V used in Additive Manufacturing











In the figure 12, are presented the mechanical properties of Ti6Al4V used in Additive Manufacturing, for different temperature domains. The chemical composition of Ti6Al4V used in Additive Manufacturing is given in the figure 13. In the figure 14, the physical properties of Ti6Al4V used in Additive Manufacturing, for different temperature domains.

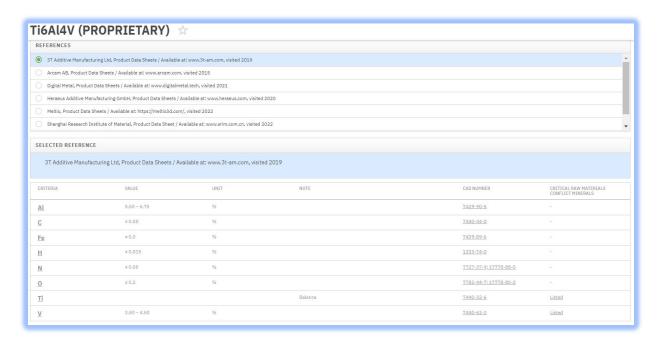


Fig.13. Chemical composition of Ti6Al4V used in Additive Manufacturing

| TEMPERATURE | PROPERTY / VALUE | |
|------------------------|--|--------------------------------|
| □ >300°C | MODULUS OF ELASTICITY | 100 — 124 GPa |
| ☐ 100 - 300°C | DENSITY | ≥ 2.5 kg/dm³ |
| 30 - 100°C ✓ 0 - 30°C | COEFFICIENT OF THERMAL EXPANSION (CTE) | 7.6 – 7.9 10 ⁻⁶ /°C |
| □ <0°C | MELTING TEMPERATURE | 1600 - 1750 °C |
| • | | |

Fig.14. Physical properties of Ti6Al4V used in Additive Manufacturing









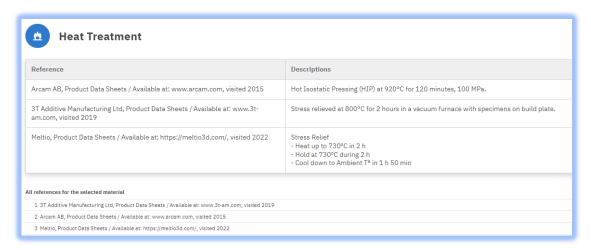


Fig.15. Heat treatment used for the alloy Ti6Al4V used in Additive Manufacturing

The database gives us details concerning the heat treatment used for the alloy Ti6Al4V used in Additive Manufacturing, as in the figure 15.



Fig.16. Metallography details for Ti6Al4V powders used in Additive Manufacturing











Total Materia gives us details concerning the metallography of the alloy Ti6Al4V used in Additive Manufacturing, as in the figure 16 and the tribology is given in figure 18. In figure 17 are presented the similar materials with the same composition existing on the market.

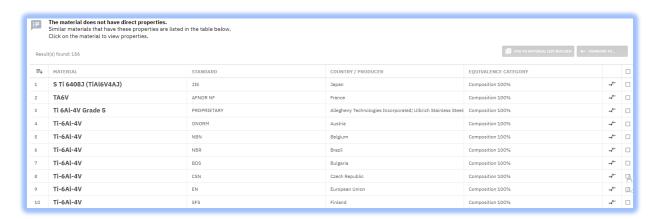


Fig.17. Similar Materials with the same composition existing on the market

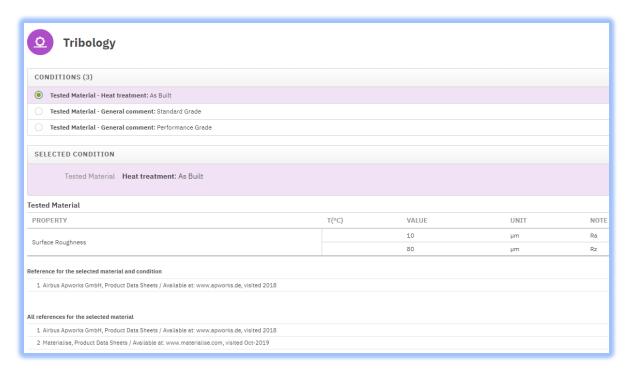


Fig.18. Tribology properties of Ti6Al4V used in Additive Manufacturing











For welding and brazing are given different variants similar alloy of Ti, as in figure 19. In the figure 20, it is presented the stress strain diagram for Ti6Al4V used in Electron Beam Melting (EBM). The fatigue data is given in the figure 21, by ARCAM company.

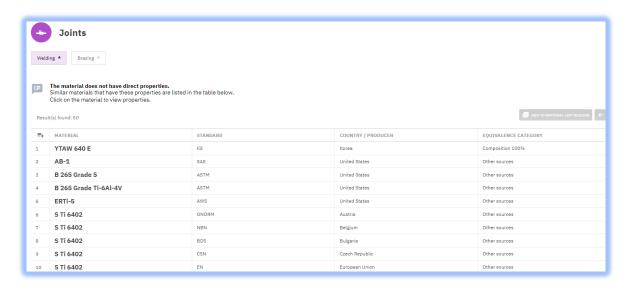


Fig.19. Different variants similar alloy of Ti, used in welding and in brazing

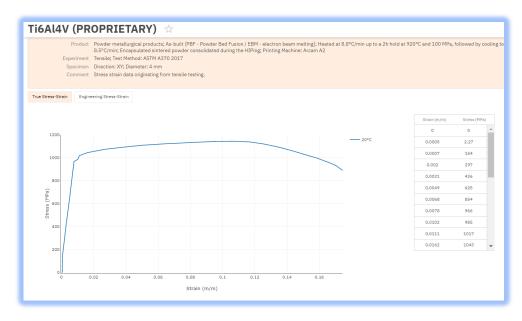


Fig.20. Stress strain diagram for Ti6Al4V used in Electron Beam Melting (EBM)











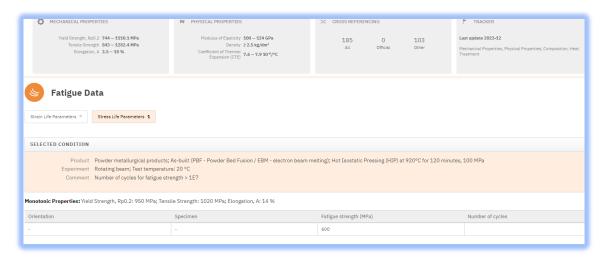


Fig.21. Fatigue data given for Ti6Al4V used in Electron Beam Melting (EBM)



Fig.22. Equivalents finder

The database permits us to find equivalents finder in function of the Brinell hardness [HB], Rockwell hardness [HR], Yield strength Rp0,2 [MPa], elongation A [%], tensile strength [MPa], reduction of area [%], Vickers hardness [HV], modulus of elasticity [GPa], density [kg/dm³], melting temperature [°C], coefficient of thermal expansion (CTE) (10-6/°C) or chemical composition, as in figure 22.

Total Materia give us the material description for the alloy Ti6Al4V used in Electron Beam Melting (EBM), specifying the applications domain, in the case of powder, is given the particles size distribution, additive laser manufacturing systems type that used this powder, the biocompatibility, as in figure 23.







| Material Description | | Application | It is used in a variety of medical applications which require high strength. | | |
|----------------------|--|---|--|--|--|
| | | Source | Oligital Metal (part of Higgeria Group Company) | | |
| | | | Connert | 30 printing (Additive narulacturing) – Sindar Verlang Machine SM P2000 | |
| Source | Meltio | | Source | Mitefalise | |
| Comment | Machine: Melti | ddfilve manufacturing) - Direct Energy Deposition (DED) o M450 with high strength, low density, high fracture toughness, excellent corrosion resistance and superior biocompatibility | Comment | 30 yrining kätile en tardischingt. Jimes Theal Lauer Serienig DIMS. Tilburn alle that mothine excellent en kehn sich serieni großes eine Heine verber en eine Ambien eine Serienische eine Serienische Heine Serie | |
| Application | Tools and prot | otypes, aerospace, marine, chemical | Application | Aeronautics, functional prototypes, solid end-use parts, medical fesions and speep parts | |
| Source | Optimal Mater | rial Technology CO.,Ltd | Source | Arcan NB | |
| | 3D printing (Additive manufacturing) - Selective Laser Melting (SLM) Machine: Concept Laser M2, EGS M 280. | | Comment | 33 yirling hiddine marketung. Tanian alay vith the high steept, god nachealids, low selpt raise ad outsteeling comsion existane. | |
| Comment | | ity, low oxygen content and good fluidity. | Application | Typically used for direct manufacturing of parts and prototypes for racing and earnsquee industry, biomechanical applications, such as impliants and protifesis, mainte applications, chemical industry, gas turbon | |
| | Hall flow rate: | stribution: 15-53 µm. 36 s/50g | Source | Sitavia | |
| Source | Shanghai Res | earch Institute of Materials | Comment | 31 princy (Editive nanolacturing - Times Meesa Exercis (DMS) Carosian resistans, streptil, herpesture esistans and reight reduction. | |
| | | 3D printing (Additive manufacturing) - Selective Laser Melting (SLM), Electron Beam Melting (EBM) | | Sonderje sp. z n.a. | |
| Comment | Particle size range: 15-45 µm. Particle size distribution d ₉₅ ≤ 30 µm. Liquidity Flowability: ≤ 40s. | | Connect | 30 yrdnog Beldin e markestuning. Sekesiek Laer Melting SJM) Tominn alloy provide. | |
| Source | Proto Labs, In | | | AURIUS APWORKS GebH | |
| Comment | 3D printing (Ad | ting (Additive manufacturing) - Direct Metal Laser Sintering (DMLS) ical properties of Tri6A4V are comparable to wrought trianium for tensile strength, elongation, and hardness. | | 30 princy (Addine marketuring 4 zeer howde Sel Addine Lee Marketuning (AM) Light weight beinn also proude Scolent mechanical properties and correction existence. Smaller wall followes (mm) (1.1) | |
| Application | It is used in a v | in a variety of medical applications which require high strength. | | Aerospace, motor sacing, and also for the production of biomedical implants. | |
| ource | purce Heraeus Additive Manufacturing GmbH | | | | |
| Comment | 3D printing (Additive manufacturing) - Laser Powder Bed Fusion (PBF-LB) High strength titanium alloy with low weight, good biocompatibility and high corrosion resistance. Particle Size Distribution (μm): 15-45 and 15-53 | | | | |
| pplication | tion Medical, aerospace and automotive | | | | |
| ource | 3T Additive Manufacturing Ltd (former 3T RPD Ltd.) | | | | |
| Comment | 3D printing (Additive manufacturing) - Direct Metal Laser Sintering (DMLS) Machine: EOSINT M290, EOSINT M280, EOSINT M400, EOSINT M400-4 Titanium alloy powder. Corrosion resistance, lightweight, biocompatible, weldable. | | | | |
| pplication | plication Prototyping, engineering, biomedical implants, small series production | | on | | |
| ource | | Vday Additive Manufacturing Technology Co., Ltd. | | | |
| omment | 3D printing (Additive manufacturing) - Selective Laser Melting (SLM), Electron Beam Melting (EBM) Titanium alloy powder. High strength to weight ratio, good mechanical properties, excellent corrosion resistance, good biocompatibility | | | | |
| | | | | | |

Fig.23. Material Description - for Ti6Al4V used in Electron Beam Melting (EBM)

In the figure 24, it is presented how can discovery the material type, choosing the domain for Brinell Hardness [HB], for the temperature 0-30°C on X axis, meaning from 500 to 800, and the compression modulus [GPa], for the temperature 0-30°C, from 100-124, and are given 2 group types, ferrous alloys and nonferrous alloy. In figure 25, the database permits us to see the material properties if it is known the standard ASTM, the standard number.











Fig.24. Material discovery



Fig.25. Standard list

3. Total Materia database – Search algorithms used for identification the unknown metallic materials

For the chemical composition Co 54,31 %, Cr 23,08 %, Mo 11,12 %, W 7,85 %, Si 3,35 % and Mn, Fe < 0,1, using the algorithms of the Total Materia database, it will identify the material with this chemical composition, as in the figures 26 and 27.

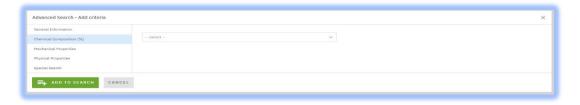


Fig.26. Algorithms used for identification the unknown materials











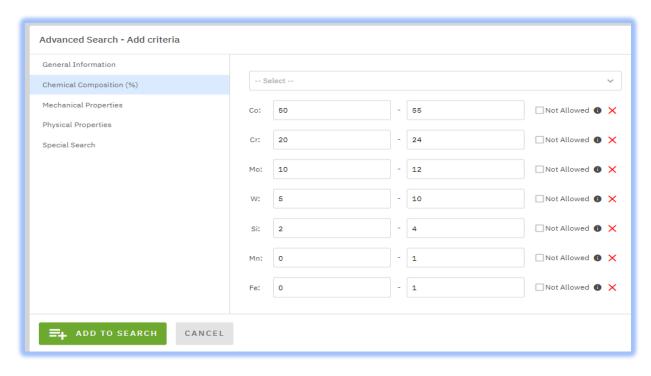


Fig.27. Chemical composition selection

When we want to change the chemical composition, it must click on clear.

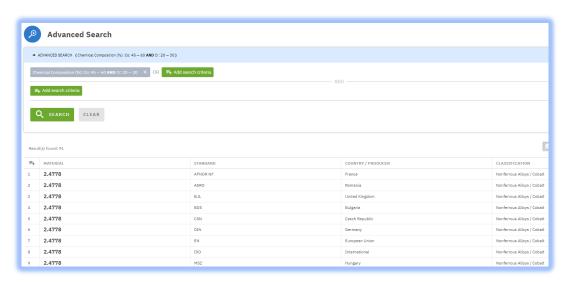


Fig.28. Co-Cr alloy results that have the respective chemical composition

In the figure 28 are presented the Co-Cr alloy results that have the respective chemical composition.











The first is the material 2.4778, standard AFNOR NF, France and if we give click, can know the mechanical properties, the chemical composition, and its applications. In the figure 29 is presented the determination of the material: CoCr28 and their properties. The material description is presented in the figure 30.

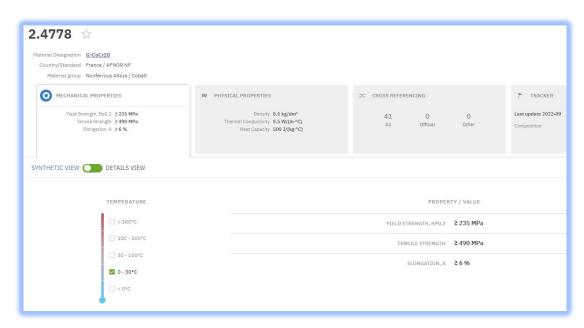


Fig.29. Determination of the material: CoCr28 and their properties



Fig.30. Material description of CoCr28











4. Total Materia database – polymers, ceramics and composite materials

Total Materia database is used too for the polymers (Fig.31), ceramics and composite materials.

The database given 125 results of PLA types, as in the figure 32.

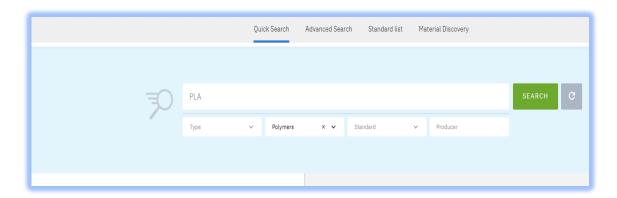


Fig.31. Total Materia database for the polymers

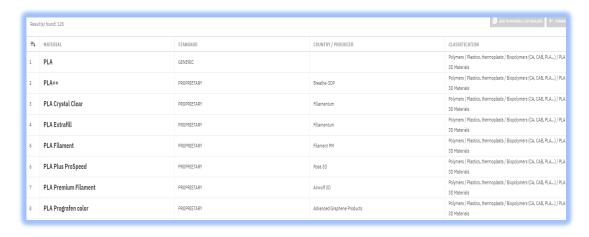


Fig.32. 125 results of PLA types existing on the database

In figure 33, are presented the mechanical properties of PLA crystal clear.

Database give us the manufacturing processes of PLA crystal clear, such as 3D Printing and temperature used in the manufacturing processes, as in figure 34.









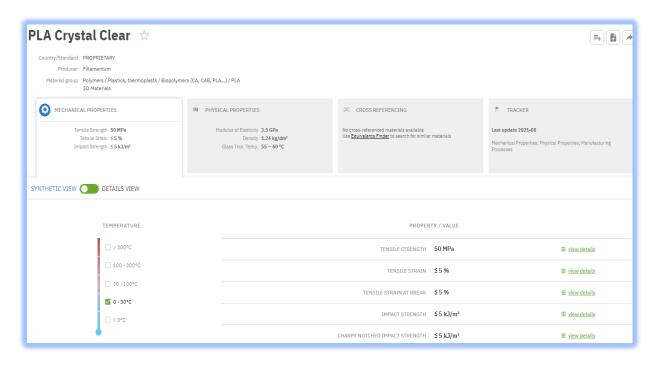


Fig.33. Mechanical properties of PLA crystal clear



Fig.34. Manufacturing processes of PLA crystal clear

In the figure 35 is realized the material description for PLA materials, being specify that it is used in Fused Deposition Modeling (FDM) process.







Fig.35. Material description for PLA filament

For ceramics, by example Hap, we obtain the results as in the figure 36.



Fig.36. Ceramic search



Fig.37. HAp variants existing on the database

In the figure 37, are given the Hap variants existing on the database, their producers, country and standards. In the figure 38 are given the mechanical properties of Hap.









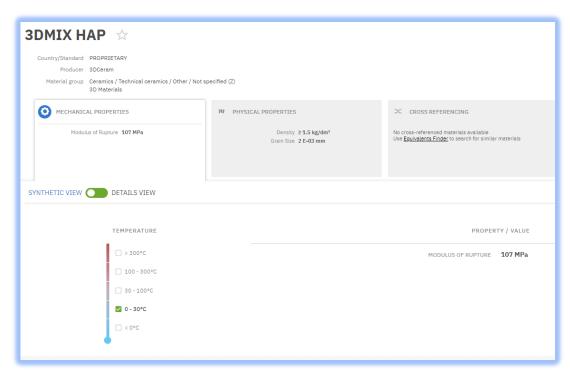


Fig.38. Mechanical properties of HAp

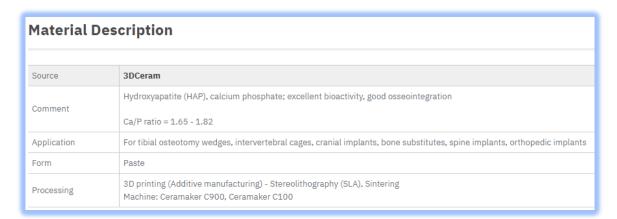


Fig.39. Material description of HAp

Hap is used in additive manufacturing in SLS and in SLA, using Ceramaker C900 or Ceramaker C100, the platform gives us inclusive information about the manufacturing systems that used this material. Hydroxyapatite is used as paste in the additive manufacturing process to obtain tibial osteotomy wedges, intervertebral cages, cranial implants, bone substitutes, spine implants or orthopaedic implants, as in the figure 39











Concerning the composite materials, by example plywood, the database give us 3 results, such in the figures 40 and 41.

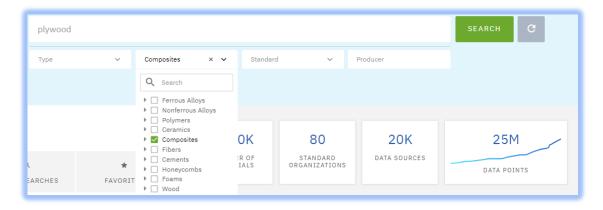


Fig.40. Quick search of plywood



Fig.41. For composite plywood – 3 results

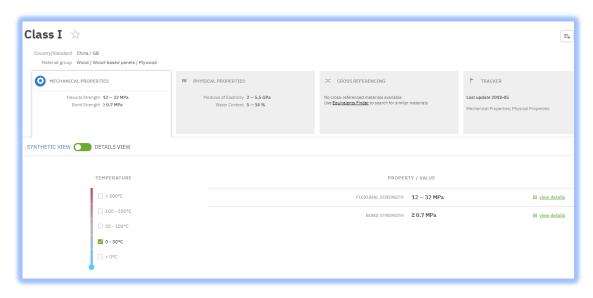


Fig.42. Mechanical properties of plywood class I







In the figure 42 are presented the mechanical properties of plywood class I. In the figure 43 is presented the material description of plywood class I, that can be used in outdoor environment.

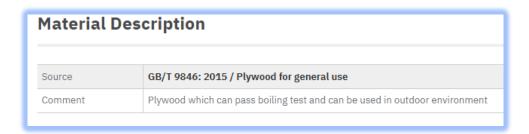


Fig.43. Material description of plywood class I

5. Conclusions

In the last years, the materials developed very much, appeared different news materials with very interesting properties realized by different world companies, that can be used in Additive Manufacturing and in other manufacturing domain to realize medical parts or for industrial domain and grace to this database, all materials developed are introduced in this platform, giving us the possibility to choose, the chemical composition, the mechanical properties, or using the search algorithms, finding the unknown material, in function of the chemical or mechanical properties.

The implications of the present research would be interesting for the manufacture by Additive Manufacturing different medical parts, using different materials using the database Total Materia, or others to know the mechanical and chemical properties that are very important to establish the manufacturing parameters and manufacturing systems and tools.

References

- 1. Ratner Buddy D., Hoffman Allan S., Schoen Frederick J., Lemons Jack E.- Biomaterials Science, An introduction to materials in medicine –Academic Press, 2013;
- 2. Materia Total database https://portal.totalmateria.com/en/search/advanced
- 3. https://link.springer.com/chapter/10.1007/978-3-662-46836-4 7











EMERALD

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EUROPEAN NETWORK FOR 3D PRINTING OF BIOMIMETIC

MECHATRONIC SYSTEMS

E-toolkit – Virtual Reality/ Augmented Reality

| Project Title | European network for 3D printing of biomimetic mechatronic systems 21-COP-0019 |
|------------------|---|
| Output | IO2 - EMERALD e-toolkit manual for digital learning in producing biomimetic mechatronic systems |
| Module | Virtual Reality /Augmented Reality (VR/AR) |
| Date of Delivery | January 2023 |
| Authors | Filip GÓRSKI, PUT |
| Version | v1, 26.01.2023 |









| 1 | Introduction | 3 |
|---|--|----------------------------|
| 2 | Building Augmented Reality applications | 4 |
| | 2.1Introduction to Unity and Vuforia Engine | 4 |
| | 2.1.1 Task 1. Preparing Unity project for work with AR.2.1.2 Task 2. Importing 3D models and preparation of AR visualization2.1.3 Task 3. Adding simple interactions.2.1.4 Task 4. Compiling the application and testing it on a tablet. | 5 8 9 13 |
| | 2.2 Creating Augmented Reality configurator of a prosthesis | 14 |
| | 2.2.1 Task 1. Preparing Unity project for work with AR.2.2.2 Task 2. Importing the 3D model for AR and applying material | 14 14 |
| 3 | Building Virtual Reality applications | 30 |
| | 3.1 Introduction | 30 |
| | 3.1.1 Task 1. Introduction - creating a SteamVR compatible project 3.1.2 Task 2. Importing a 3D model and creating a scene 3.1.3 Task 3. Product configuration programming 3.1.4 Task 4. Animation programming 3.1.5 Task 5. Creating an executable application. 3.2 Creating a configurator for own model (own work) | 31 35 38 46 51 |
| | | |
| 4 | Summary | 53 |

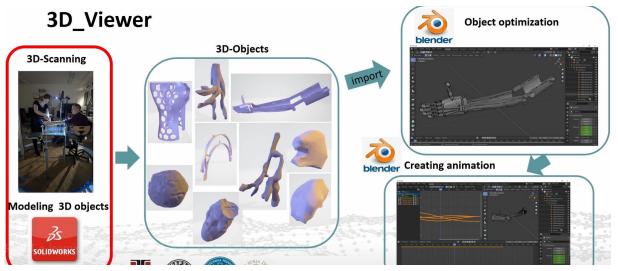








1 Overview of whole process



To create the 3D preview in Augmented reality we need 3D objects, we can get this through following steps:

- 3D scanning
- Or modeling of the 3D objects

Then there is a process which involves object optimization and creating animation.

Here we can see the scanning scanning of a hand in detail:



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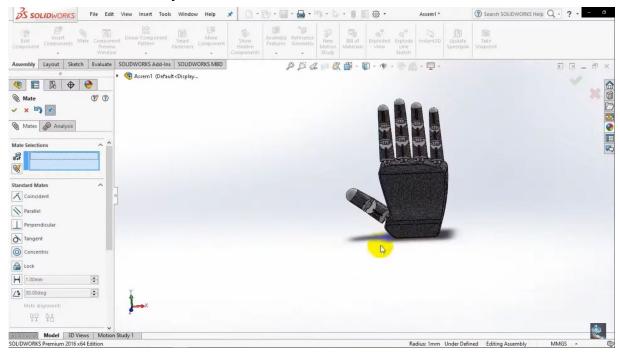




2 Building Augmented Reality animations

Introduction to Blender software

We can also model an object in software called SolidWorks or similar.



If we have the object in as a 3d object, we need to import them into program where we're going to optimize these – in our example we use Blender.

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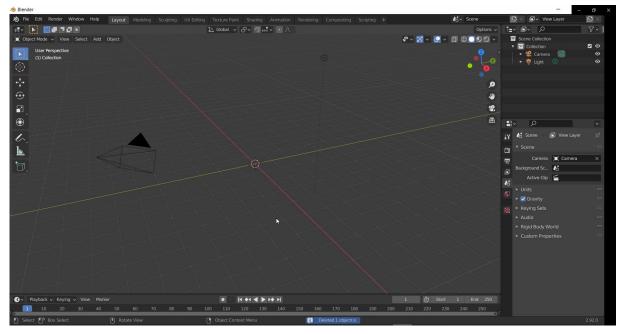




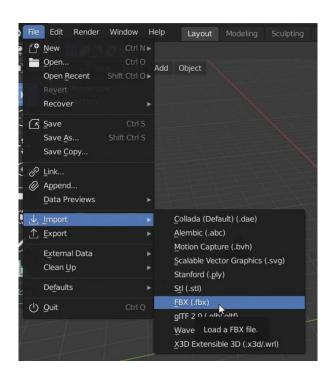


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That means if we have a vertex files, we can create animation in Blender software. This is a simple process where we import the model first:





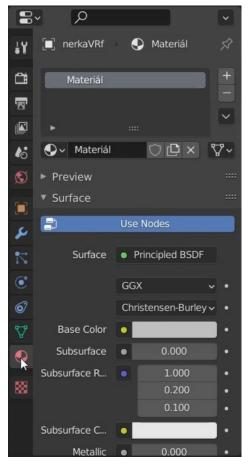




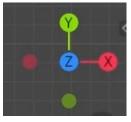




We can change the materials or specifications of the object we will switch to view specifically color palette of this object in right bottom corner:



We have different axis in top right corner:



And from the bottom of the screen we can expand the timeline where we can create individual frame.

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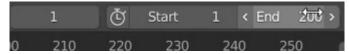


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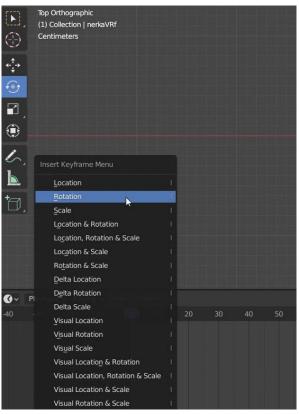




We will set the starting and ending of the timeline



On the first second of timeline, we will create a first frame of the rotation through axis y – by pressing the KEY button "I". Then selecting Rotation from the Edit Mode, or by pressing "R" we rotate the object through axis y.



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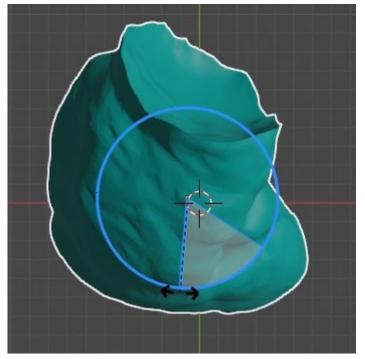






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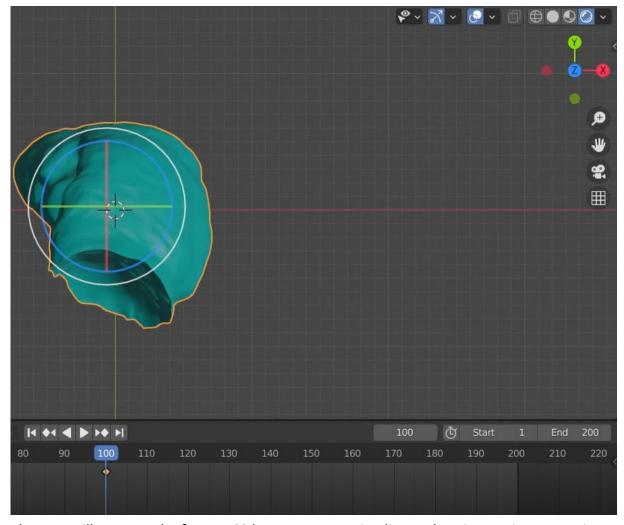
We will fix this position at 100. This means we will move to frame 100 with mouse and then rotate the object by pressing "R" and then pressing the KEY button "I" to fix it.











Then we will move to the frame 160 by mouse over Timeline and again rotating over axis y we rotate the object. And again, we will fix the position and by pressing "I" then moving to the last one at 200, rotating object again by "R". We will fix the position.

If we are unsatisfied with specific frame, we can remove it With DELETE key and we can replace it, we need to rotate the object according to the axis Zed Z. And we can fix it again at this position on the timeline.



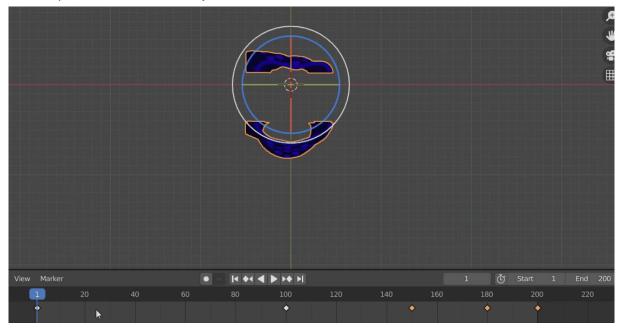








Here is preview of another object where we created another animation:



We can also create more complex animations.

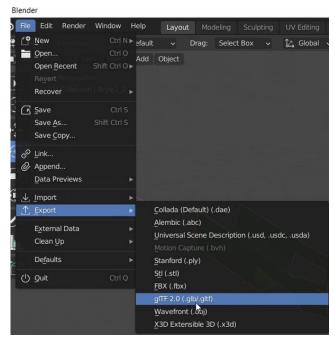
Once we have the objects created, we need to save them and export them into Glb file for Android.











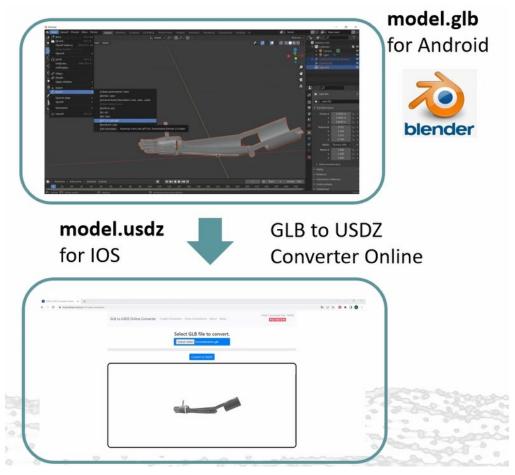
Or we can use the USDZ format, which is for IO OS, we can find the online core value converter for such.



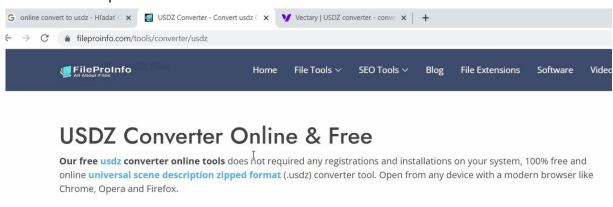








And here is the preview of online converter to create USDZ file.



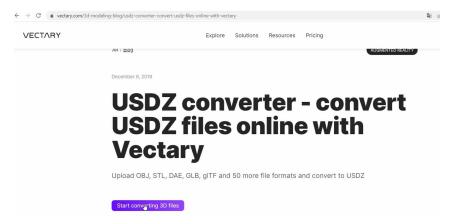








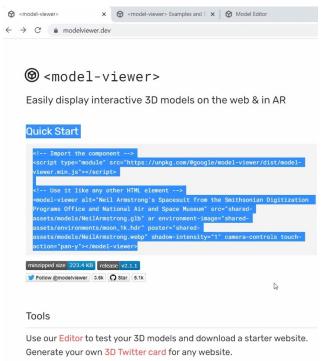




Creating website to display AR models

Once we have the individual models, we use the web interface WEB APP - 3D Viewer, which is used to create preview of the 3D models using the HTML code.

At www.modelviewer.dev we have the documentation and examples. This documentation is right iterated to the specific model viewer. And we can utilize the https://modelviewer.dev/editor/ where we can test our code, there are some examples from where we can get an inspiration.





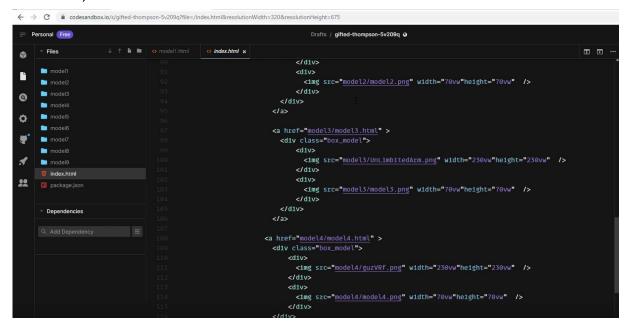






Once we have the code, we need to publish it. Either this could be own web server or it could be a code sandbox where we will publish our code. It's free it only requires registration at https://codesandbox.io/

There we can start a website. Here in our example we can see specific environment where we have index, which is a main site.



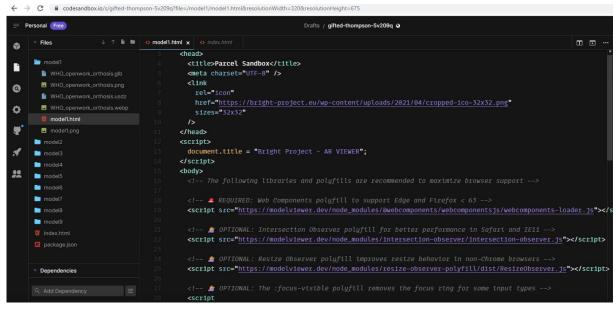
Through this we can redirect to other imported sub models. As you can see from the screenshot, it contains the models. For example, here we can click on the first object model1.html:











The sub site of the first object contains individual code as well.

The site will generate from 3Dmodel html code a model displayed in augmented reality, either Android or iOS. Which we can click, we can rotate it and interact with.

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